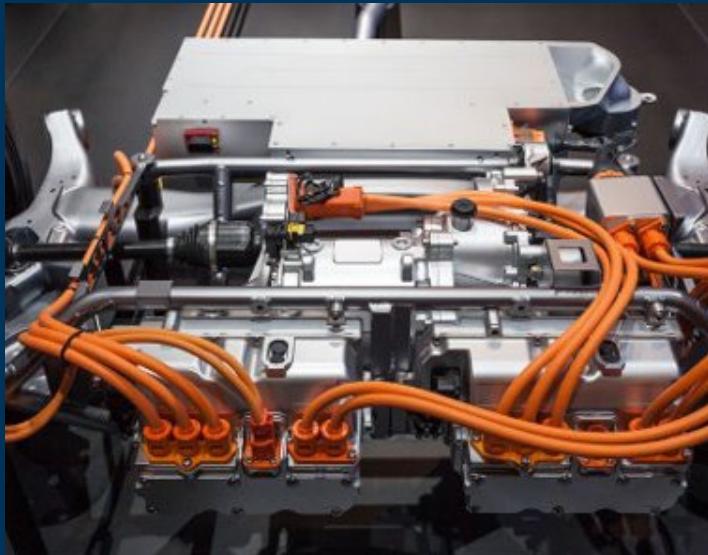




HBM Prenscia Technology Day

Virtual Seminar Series



Analysis of Electric Powertrain Measurements – Torque, Power, Efficiency, Vibration

Presented by Dr. Andrew Halfpenny
Chief Technologist, HBM Prenscia
HBK

Session #2: Electrical Power Testing & Analysis

Analysis of Electric Powertrain Measurements – Torque, Power, Efficiency, Vibration

Abstract

The theoretical and real-world range of an electric vehicle may differ significantly. To maximize the range and overall efficiency of the vehicle, it is necessary to understand and characterize how the vehicle is used and determine through meticulous measurement and analysis where efficiency losses occur.

Quantifying AC power is particularly difficult. Unlike the conventional electricity grid, electric vehicles convert DC to AC using an electrical inverter. Using pulse-width modulation, these produce a frequency-modulated, non-sinusoidal, transient waveform. This presentation introduces the concept of AC power analysis post-processing. Starting with steady-state sinusoidal waveforms, it explains the basic concepts of Active, Reactive, Apparent Power, and the Power Factor. It then considers the effect of non-sinusoidal and transient waveforms. Digital Signal Processing (DSP) techniques are introduced that take advantage of high-speed digitized data.

The presentation covers the following methods of AC power analysis - Time-averaging methods: Windowed-statistical method - time domain, PSD/CSD method - frequency domain; Instantaneous methods: Clarke transform method - time domain, Hilbert transform method - frequency domain. A case study shows the advantages of each method based on real data from an electric vehicle.

About the presenter, Dr. Andrew Halfpenny

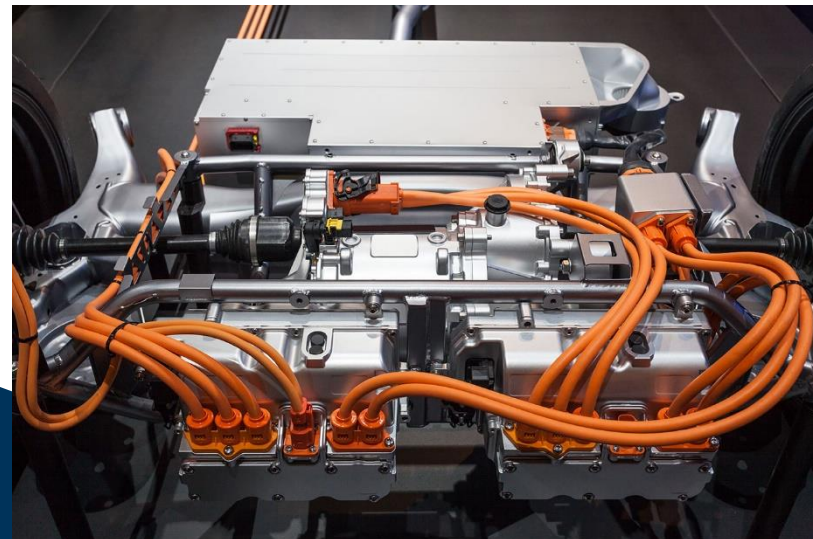
Dr. Halfpenny has a PhD in Mechanical Engineering from University College London (UCL) and a Masters in Civil and Structural Engineering. With over 25 years of experience in structural dynamics, vibration, fatigue and fracture, he has introduced many new technologies to the industry including: FE-based vibration fatigue analysis, crack growth simulation and accelerated vibration testing. He holds a European patent for the 'Damage monitoring tag' and developed the new vibration standard used for qualifying UK military helicopters. He has worked in consultancy with customers across the UK, Europe, Americas and the Far East, and has written publications on Fatigue, Digital Signal Processing and Structural Health Monitoring. He sits on the NAFEMS committee for Dynamic Testing and is a guest lecturer on structural dynamics with The University of Sheffield.

Analysis of Electric Powertrain Measurements – Torque, Power, Efficiency, Vibration

FOCUS ON AC POWER ANALYSIS IN ELECTRIC VEHICLES

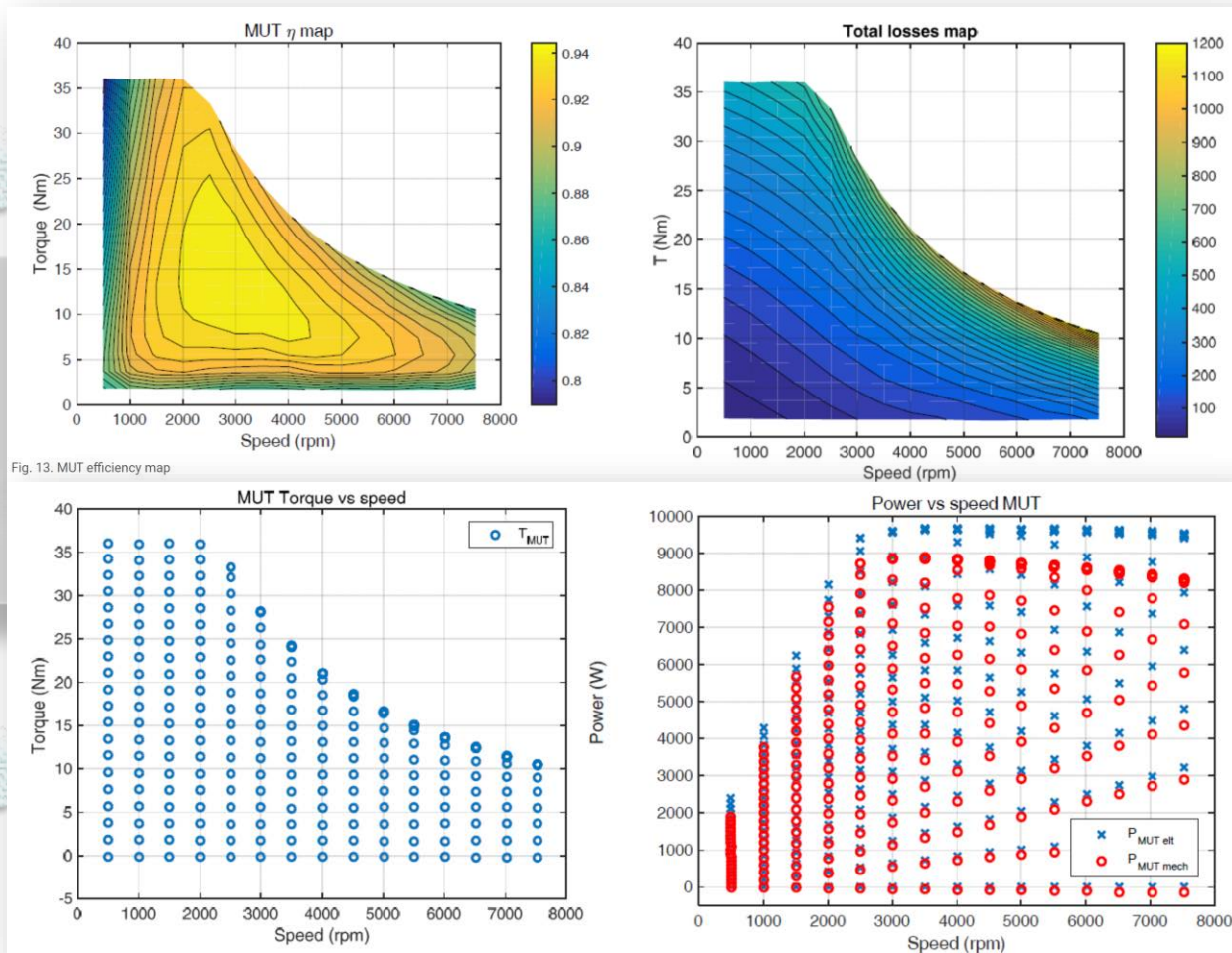
Dr Andrew Halfpenny

Director of Technology – nCode Products



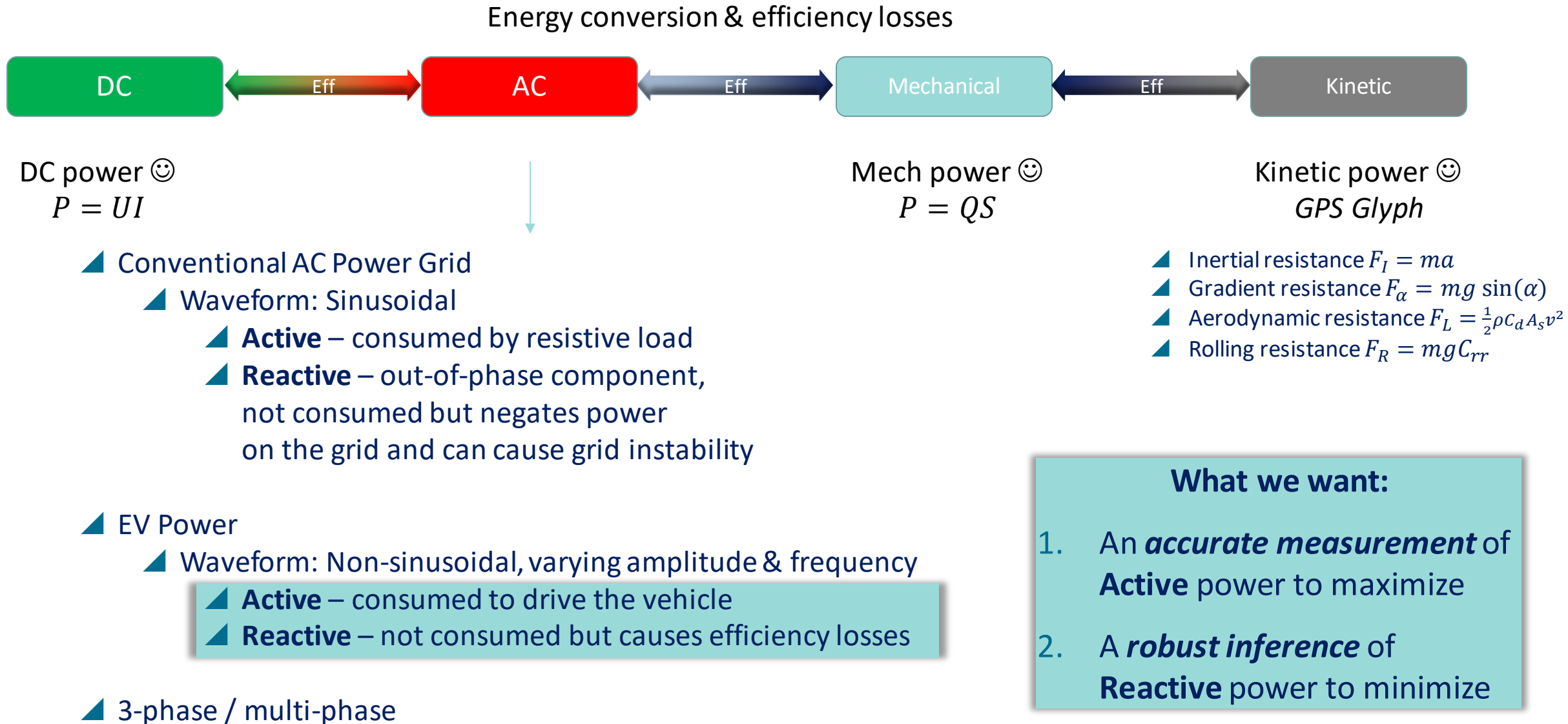
Efficiency of an Electrical Vehicle

Energy conversion & efficiency losses



- Battery DC
- Inverter DC-AC
- Motor AC
- Transmission
- Whole vehicle

Efficiency of an Electrical Vehicle



Agenda

1. Definitions for pure sine AC

- Active, Reactive, Apparent power, and the Power factor
- Analytical and Digital signal definitions

2. Inverter Analysis – *Time-averaging methods*

- Windowed-statistical method – *time domain*
- PSD/CSD method – *frequency domain*

3. Inverter Analysis – *Instantaneous methods*

- Clarke transform method – *time domain*
- Hilbert transform method – *frequency domain*

4. GlyphWorks Post-processing Case Studies

Definitions for pure sine AC

Active, Reactive, Apparent power, and the Power factor
Analytical and Digital signal definitions

Pure Sine AC: Active and Reactive Power

AC voltage: — $u(t) = U \cos(\omega t)$

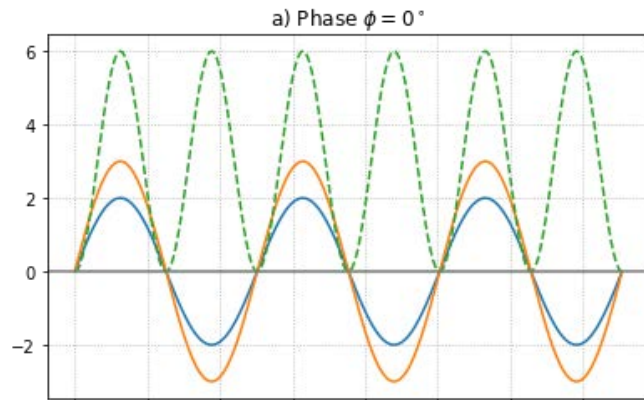
AC current: — $i(t) = I \cos(\omega t + \phi)$

Instantaneous power: — $p(t) = u(t) i(t)$

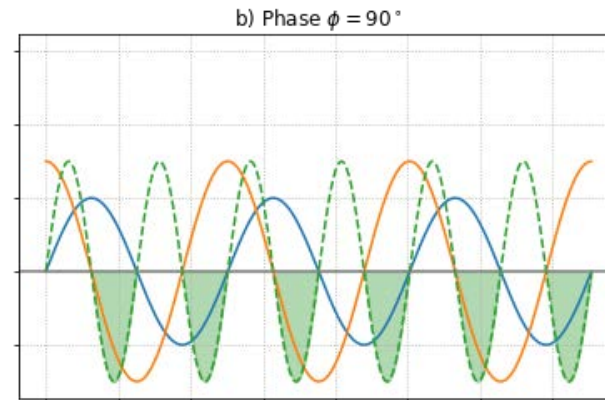
Convention:

▲ U = amplitude of voltage

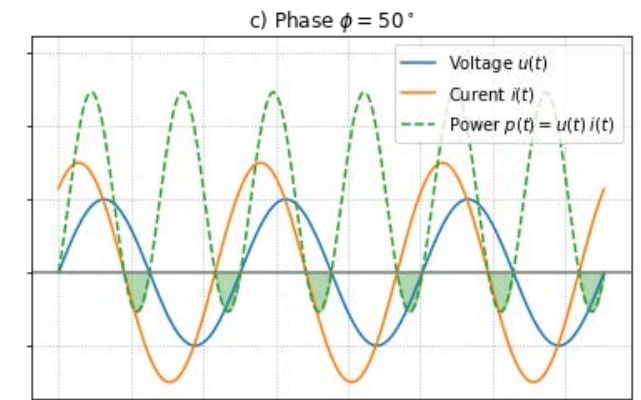
▲ I = amplitude of current



Power factor $\cos(\phi) = 1.0000$
Active power $P = 3.0000$
Reactive power $Q = 0.0000$
Apparent power $S = 3.0000$



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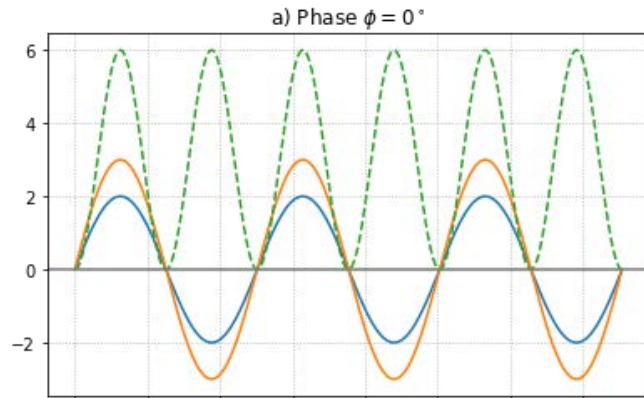
Power factor $\cos(\phi) = 0.6428$
Active power $P = 1.9284$
Reactive power $Q = 2.2981$
Apparent power $S = 3.0000$

- Instantaneous power frequency 2x input voltage and current frequency
- Instantaneous power is wholly +ve
- All energy is consumed by the load
“Resistive” load

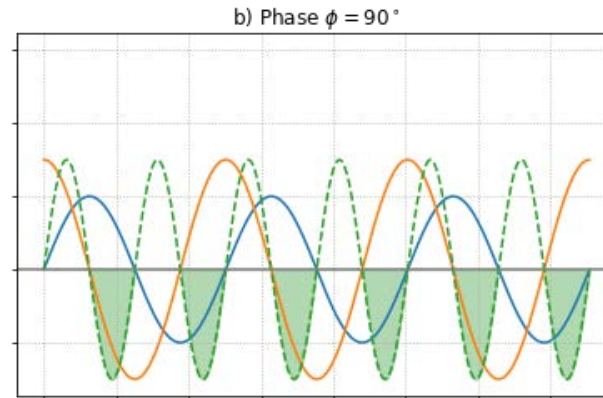
- Same instantaneous power frequency and amplitude
- Instantaneous power is equally +ve and -ve (zero mean)
- No energy is consumed by the load
“Reactive” load

- Same instantaneous power frequency and amplitude
- Instantaneous power has some +ve and -ve (non-zero mean)
- Some energy is consumed, some is not
“Active” and “Reactive” load

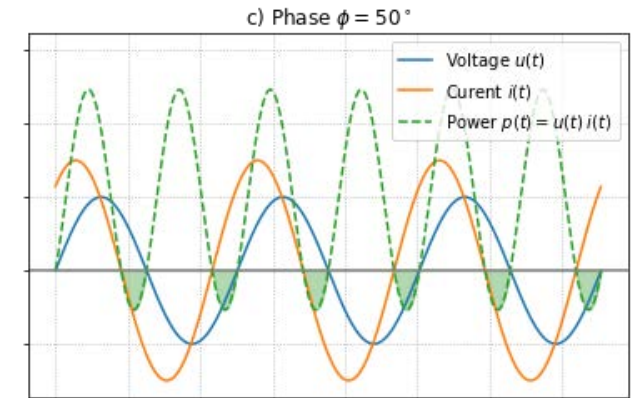
Pure Sine AC: Active and Reactive Power



Power factor $\cos(\phi) = 1.0000$
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Power factor $\cos(\phi) = 0.6428$
 Active power $P = 1.9284$
 Reactive power $Q = 2.2981$
 Apparent power $S = 3.0000$

$$\begin{aligned}
 p(t) &= u(t) i(t) \\
 &= U \cos(\omega t) \times I \cos(\omega t) \\
 &= UI \cos^2(\omega t) \\
 &= \frac{UI}{2} [1 + \cos(2\omega t)]
 \end{aligned}$$

↑ ↑ ↑
 Makes it +ve Frequency 2x input
 Amplitude (Apparent power)

Wholly resistive load: PF = 1

$$\begin{aligned}
 p(t) &= u(t) i(t) \\
 &= U \cos(\omega t) \times I \sin(\omega t) \\
 &= \frac{UI}{2} [\sin(2\omega t)]
 \end{aligned}$$

- Same Apparent power
- Same frequency
- Zero mean
equal +ve and -ve

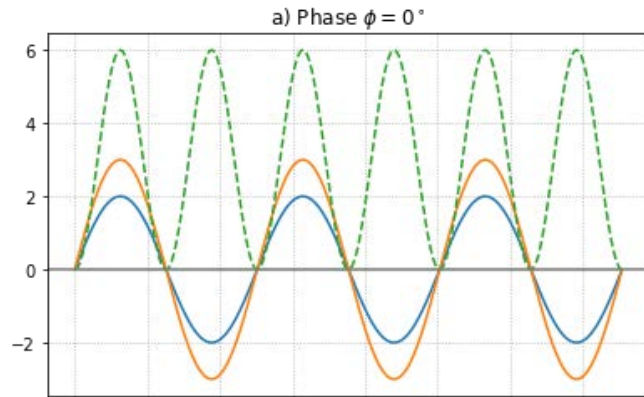
Wholly reactive load: PF = 0

$$\begin{aligned}
 p(t) &= u(t) i(t) \\
 &= U \cos(\omega t) \times I \cos(\omega t + \phi) \\
 &= \frac{UI}{2} [\cos(2\omega t + \phi) + \cos(\phi)]
 \end{aligned}$$

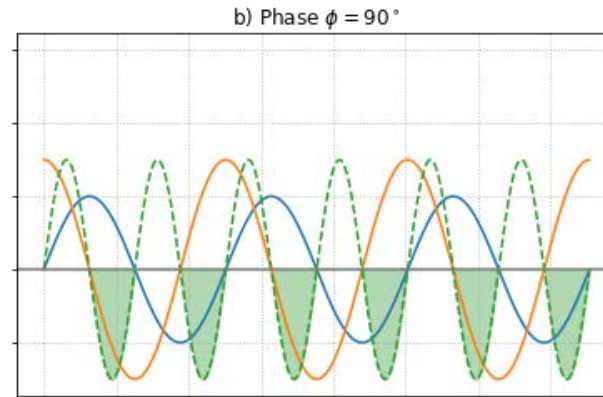
- Same Apparent power
- Same frequency
- Mean offset $\mu = \frac{UI}{2} \cos(\phi)$

$\cos(\phi)$ is known as the
 'Power Factor (PF)'

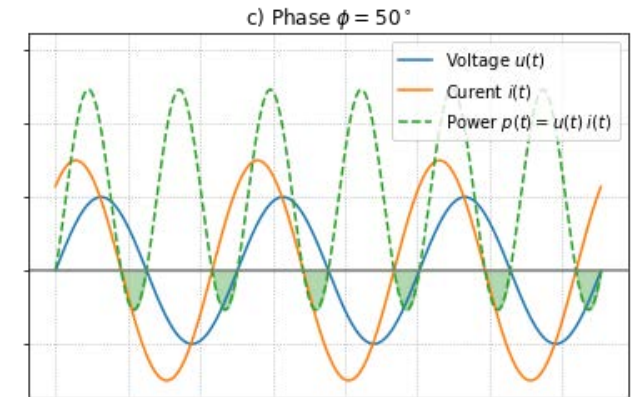
Pure Sine AC: Active and Reactive Power



Power factor $\cos(\phi) = 1.0000$
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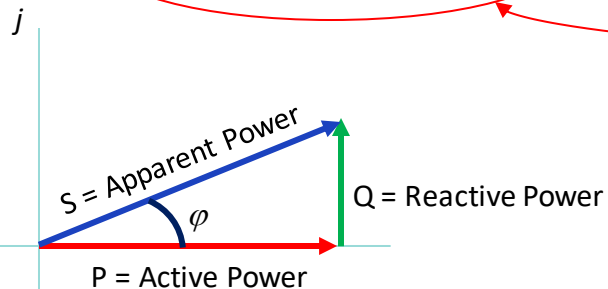
$$\begin{aligned} p(t) &= u(t) i(t) \\ &= U \cos(\omega t) \times I \cos(\omega t) \\ &= UI \cos^2(\omega t) \\ &= \frac{UI}{2} [1 + \cos(2\omega t)] \end{aligned}$$

$$\begin{aligned} p(t) &= u(t) i(t) \\ &= U \cos(\omega t) \times I \sin(\omega t) \\ &= \frac{UI}{2} [\sin(2\omega t)] \end{aligned}$$

$$\begin{aligned} p(t) &= u(t) i(t) \\ &= U \cos(\omega t) \times I \cos(\omega t + \phi) \\ &= \frac{UI}{2} [\cos(2\omega t + \phi) + \cos(\phi)] \end{aligned}$$

$$\begin{aligned} &= \frac{UI}{2} [\cos(2\omega t) \cos(\phi) + \sin(2\omega t) \sin(\phi) + \cos(\phi)] \\ &= \frac{UI}{2} \cos(\phi) [1 + \cos(2\omega t)] + \frac{UI}{2} \sin(\phi) [\sin(2\omega t)] \end{aligned}$$

Instantaneous Power $p(t)$ is the weighted sum of the **Active** and **Reactive**



Power Triangle

Amplitude

Active power	$P = \frac{UI}{2} \cos(\phi)$
Reactive power	$Q = \frac{UI}{2} \sin(\phi)$
Apparent power	$S = \frac{UI}{2} = \sqrt{P^2 + Q^2}$
Power factor	$PF = \cos(\phi) = \frac{P}{S}$

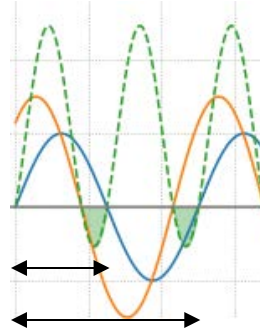
Pure Sine AC: Active and Reactive Power

$$u(t) = U \cos(\omega t) \quad i(t) = I \cos(\omega t + \phi)$$

Analytical Definitions

Active Power

$$P = \frac{UI}{2} \cos(\phi)$$



Digital Definitions

$$\text{mean}(u \times i)$$

$$P = \text{mean}(u(t) i(t)) \Rightarrow \frac{1}{N} \sum_{n=1}^N u_n i_n$$

$$= \frac{1}{2\pi} \int_{-\pi}^{\pi} U \cos(\omega t) \cdot I \cos(\omega t + \phi) dt = \frac{UI}{2} \cos(\phi)$$

Apparent Power

$$S = \frac{UI}{2}$$

$$\text{rms}(u) \times \text{rms}(i)$$

$$S = \text{rms}(u) \cdot \text{rms}(i)$$

$$\text{rms}(I \cos(\omega t + \phi)) = \sqrt{\frac{1}{2\pi} \int_{-\pi}^{\pi} (I \cos(\omega t + \phi))^2 dt} \Rightarrow \frac{I}{\sqrt{2}}$$

$$\therefore S = \frac{UI}{2}$$

Reactive Power

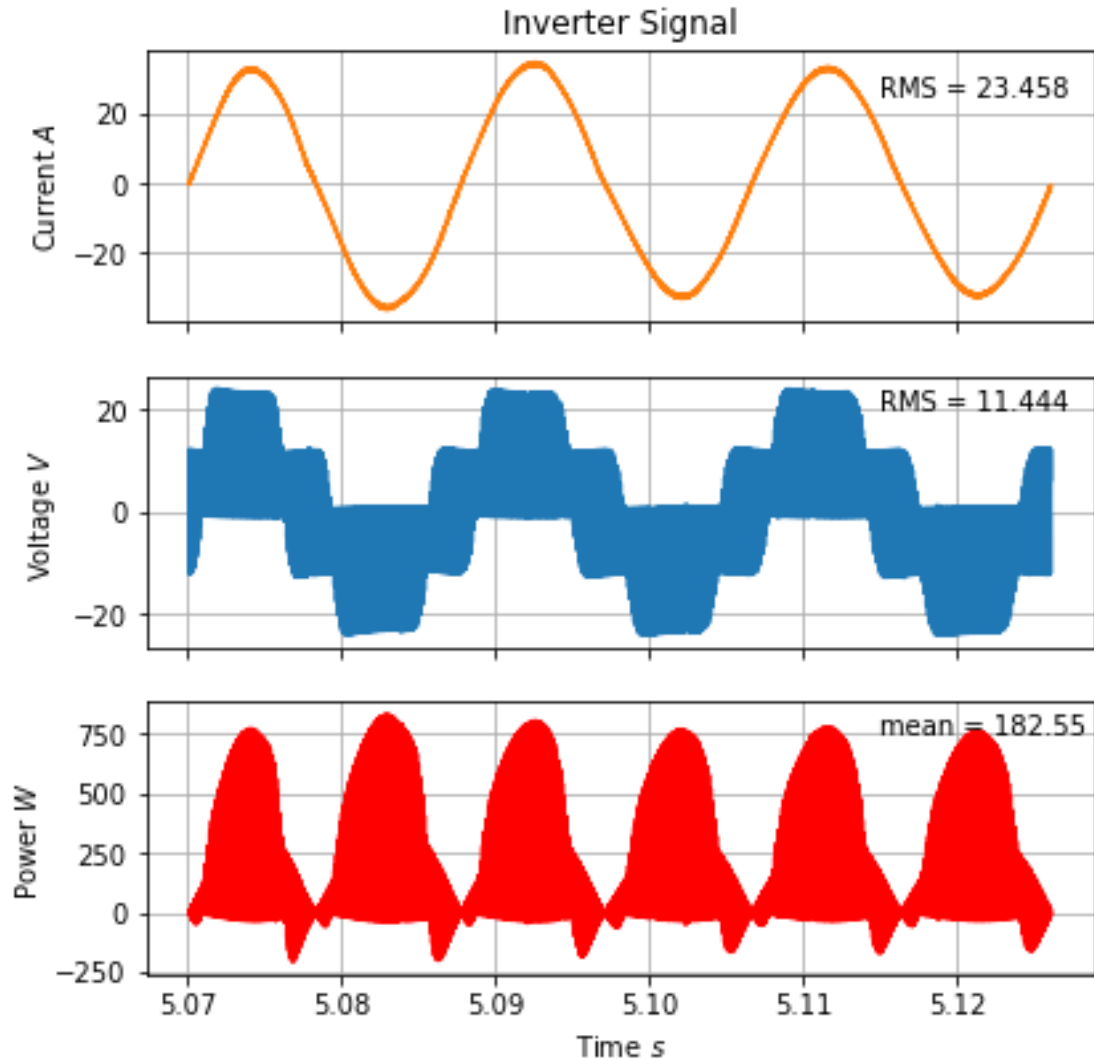
$$Q = \frac{UI}{2} \sin(\phi)$$

$$|Q| = \sqrt{S^2 - P^2} = \frac{UI}{2} \sin(\phi)$$

Inverter Analysis – *Time-averaging methods*

Windowed-statistical method – *time domain*
PSD/CSD method – *frequency domain*

Typical Inverter Signal



$$\text{Active Power } P = \text{mean}(u(t) i(t)) = 182.55 \text{ W} \quad \checkmark$$

$$\begin{aligned} \text{Apparent Power } S &= \text{rms}(u(t)) \times \text{rms}(i(t)) \\ &= 11.444 \times 23.458 = 268.45 \text{ VA} \end{aligned}$$

$$\begin{aligned} \text{Reactive Power } Q &= \sqrt{S^2 - P^2} \\ &= \sqrt{268.45^2 - 182.55^2} = 196.83 \text{ VAr} \end{aligned}$$

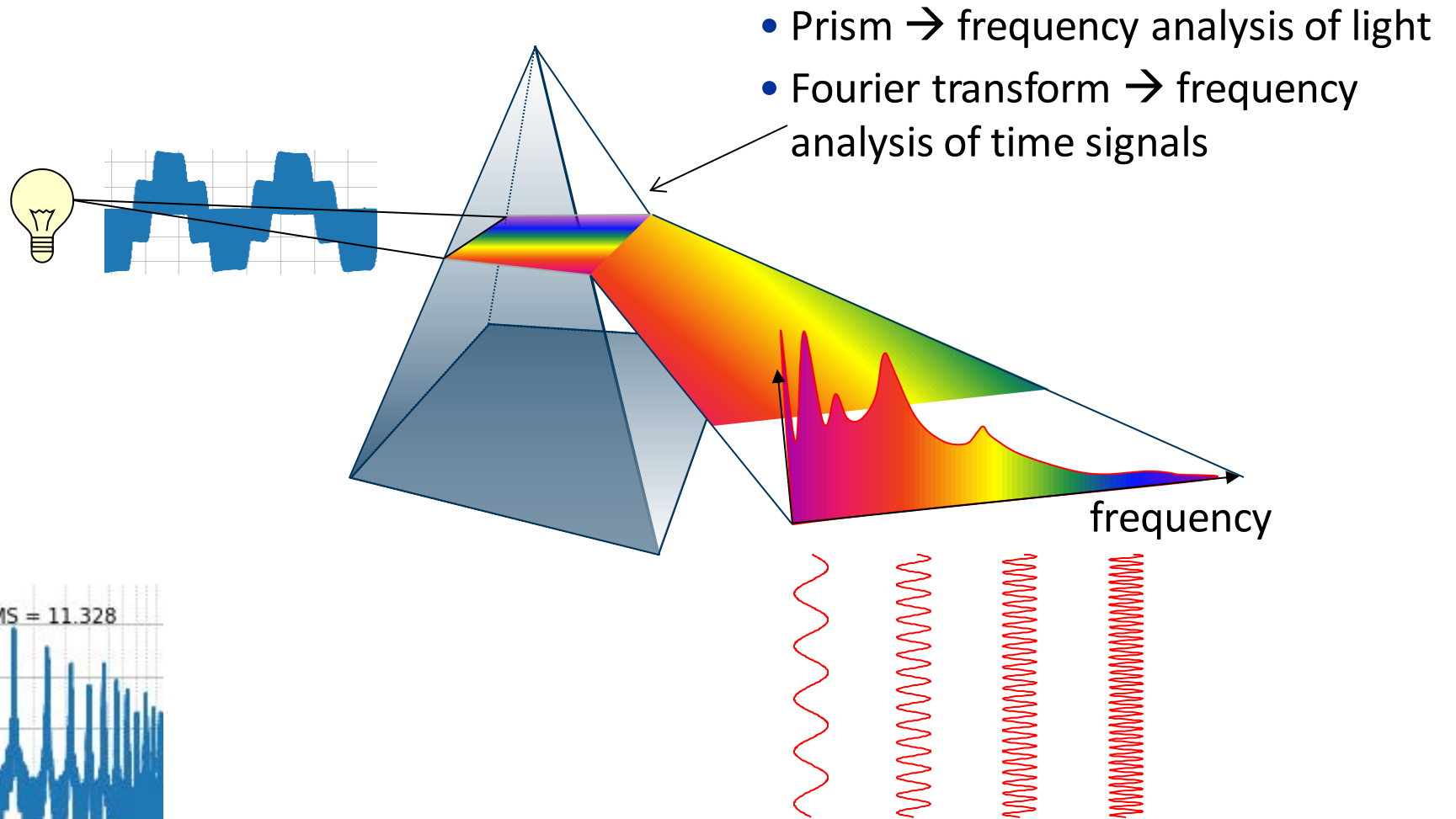
Expecting $Q \ll P$ Found $Q > P$

What's happened

- Active power is correct by definition ✓
- This definition of 'Apparent Power' merges all the frequencies together into one (*RMS*) before calculating power
- It is often more helpful to apply the calculation to each frequency separately

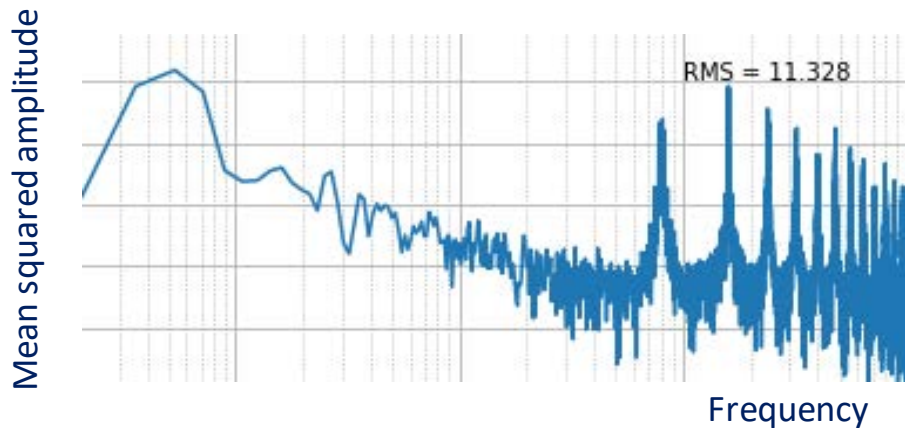
Frequency Domain Method

- Decompose inverter signal into its sinusoidal components using Fourier Transform

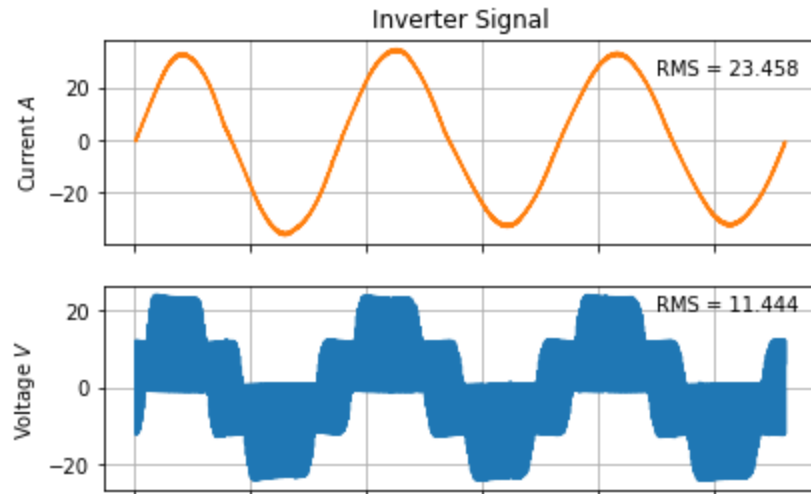


Power Spectral Density (PSD) curve

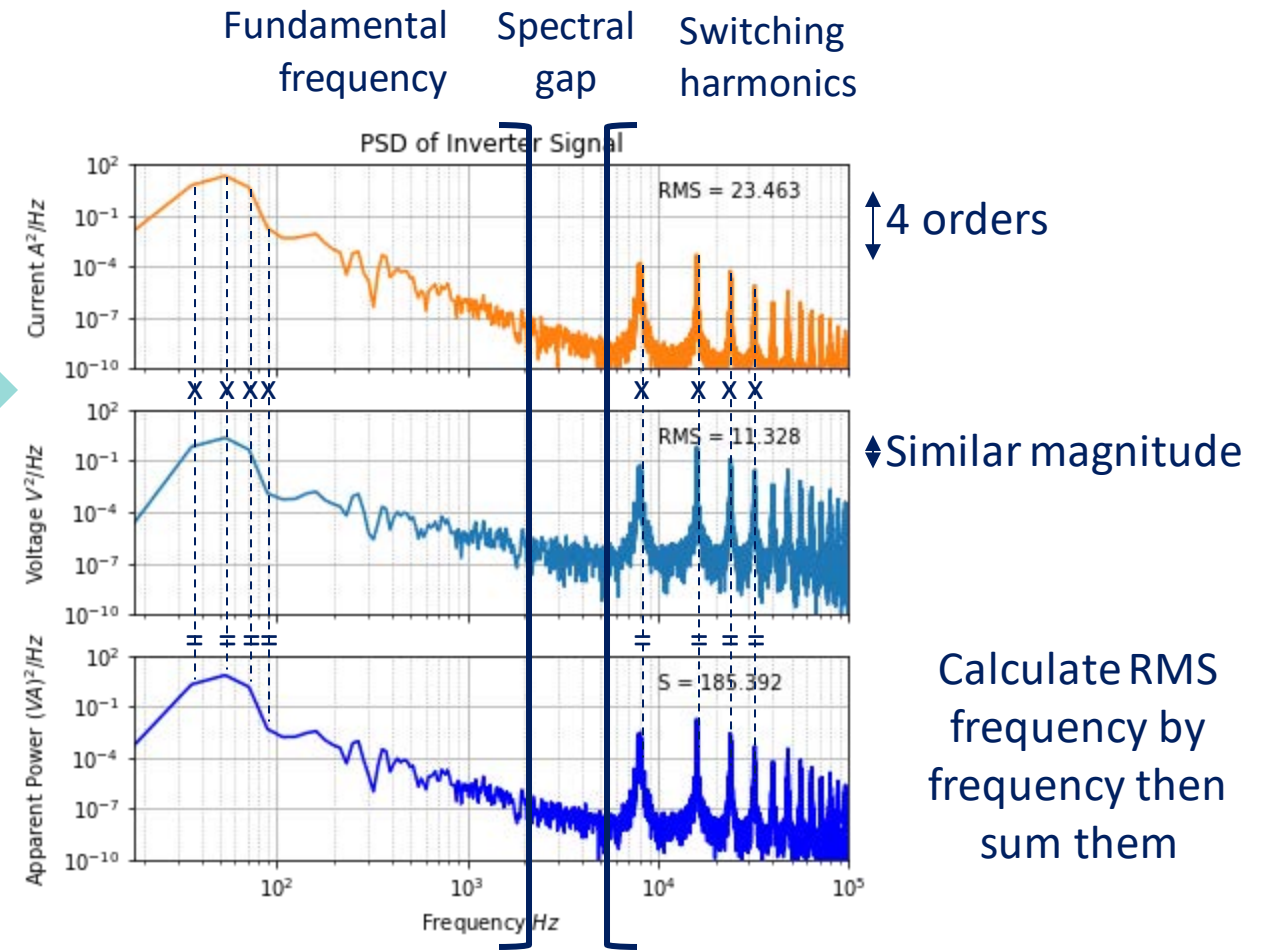
$$RMS = \sqrt{\text{Area under PSD}}$$



Frequency Domain Method – PSD



PSD



From previous page
definition 1:

$$P = 182.55 \text{ W}$$

$$S = \frac{1}{2} \sum_h U_h \sum_h I_h = 268.45 \text{ VA}$$

$$Q = \sqrt{S^2 - P^2} = 196.83 \text{ VAR}$$

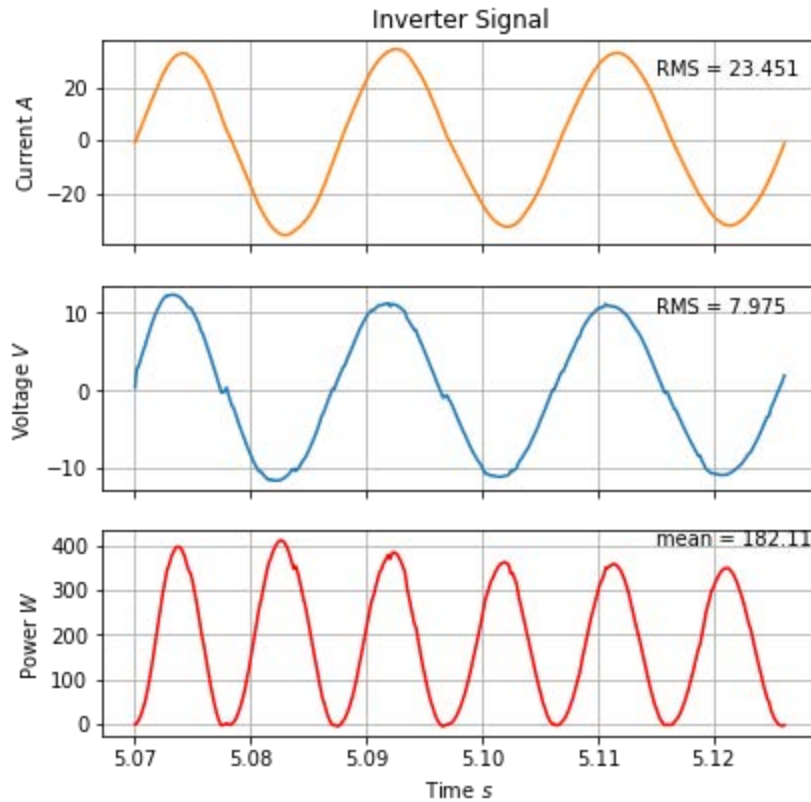
definition 2:

$$P = 182.55 \text{ W}$$

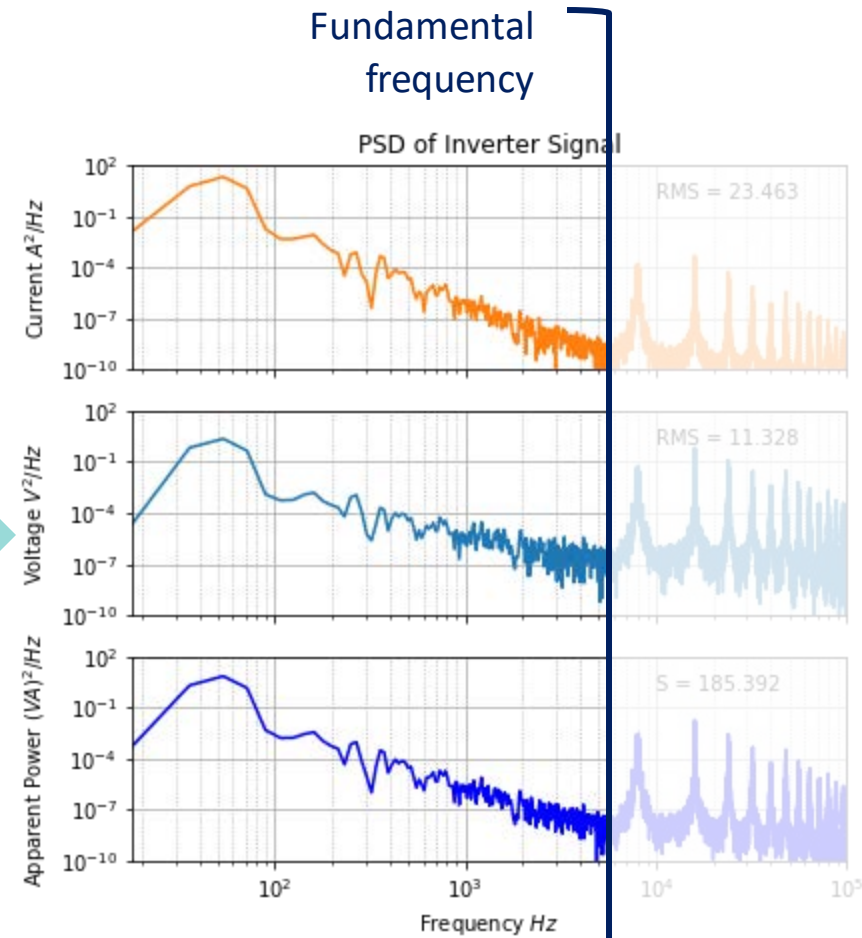
$$S = \frac{1}{2} \sum_h U_h I_h = 185.39 \text{ VA}$$

$$Q = \sqrt{S^2 - P^2} = 32.34 \text{ VAR}$$

Filtered Time Domain Method



PSD



Apparent power
definition 1:
Filtered to
fundamental

$$P = 182.11 \text{ W}$$

$$S = \frac{1}{2} \sum_h U_h \sum_h I_h = 187.02 \text{ VA}$$

$$Q = \sqrt{S^2 - P^2} = 42.57 \text{ VAR}$$

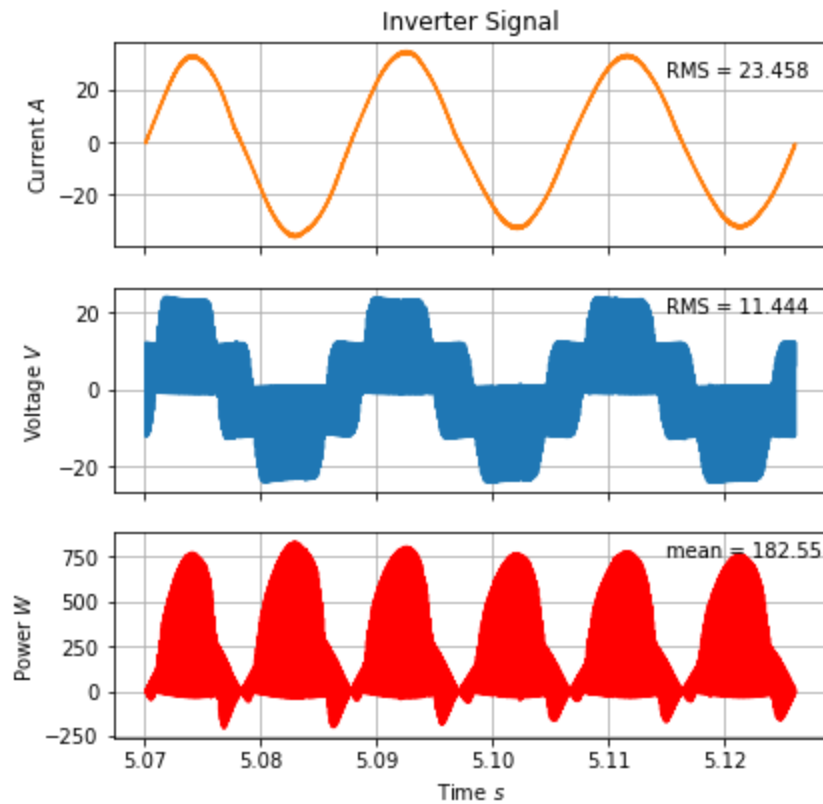
definition 2:

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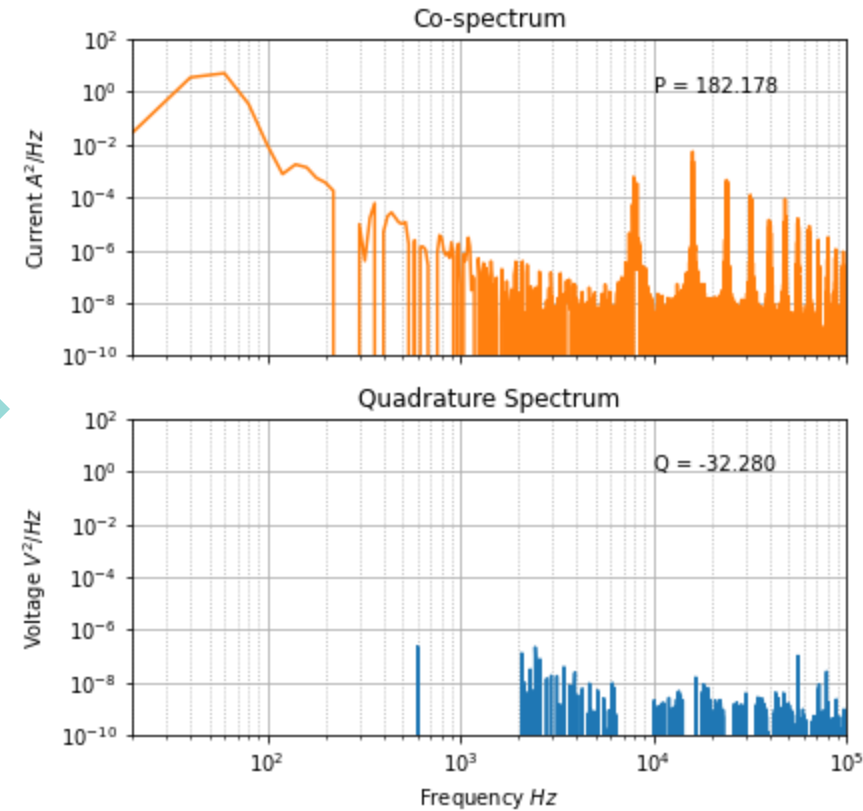
$$Q = \sqrt{S^2 - P^2} = 32.34 \text{ VAR}$$

Frequency Domain Method – CSD



CSD

P = Area under Co-Spectrum
 Q = Area under quadrature spectrum



$$P = \sum_h \frac{U_h I_h}{2} \cos(\phi_h)$$

$$Q = \sum_h \frac{U_h I_h}{2} \sin(\phi_h)$$

- mean power $\approx P = 182.178$
- $Q = -32.280$ is a more robust inference

Conclusion: Time-averaging Methods

Time-domain method

$$P = \text{mean}(i(t) u(t))$$

$$S = \text{RMS}(i(t)) \times \text{RMS}(u(t))$$

$$Q = S \sin\left(\cos^{-1}\left(\frac{P}{S}\right)\right)$$

- ▲ Pure sine method
- ▲ For preferred definition of Q, use low-pass filter to isolate the fundamental frequency
- ▲ Excellent time resolution is possible
(down to half-cycle in the best systems)
- ▲ Ideal for analysing dynamic EV systems & WLTC (Worldwide Harmonised Light Vehicle Test Procedure)



Frequency-domain method

$$P = \text{area}(\text{Re}[csd(i(t), u(t))])$$

$$Q = \text{area}(\text{Im}[csd(i(t), u(t))])$$

$$S = \text{area}(|csd(i(t), u(t))|)$$

- ▲ Broadband method (preferred definition of Q)
- ▲ Time buffer (2^n points) insensitive to cycle edges
- ▲ Large time buffer required to capture low-frequency fundamental
- ▲ Large buffer gives poor time resolution
- Not ideal for dynamic EV systems & WLTC

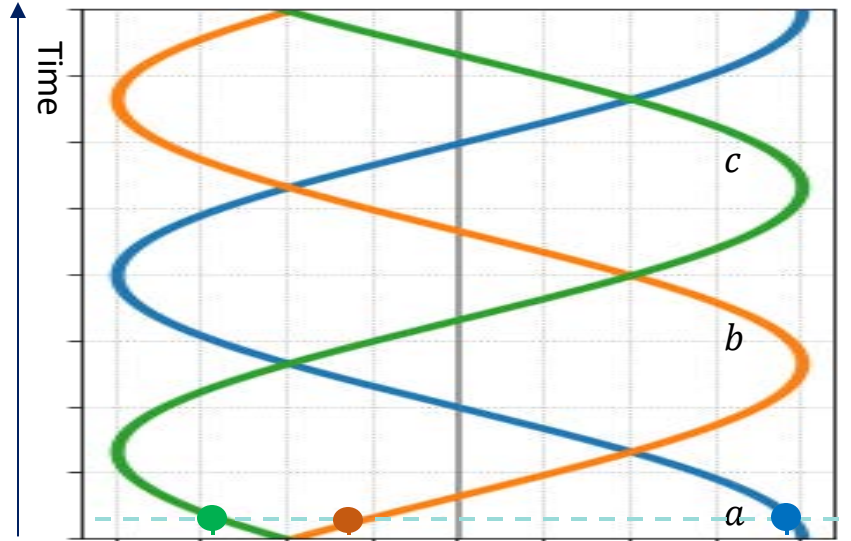


Inverter Analysis – *Instantaneous methods*

Clarke transform method – *time domain*

Hilbert transform method – *frequency domain*

Direct Quadrature Transformation – α, β

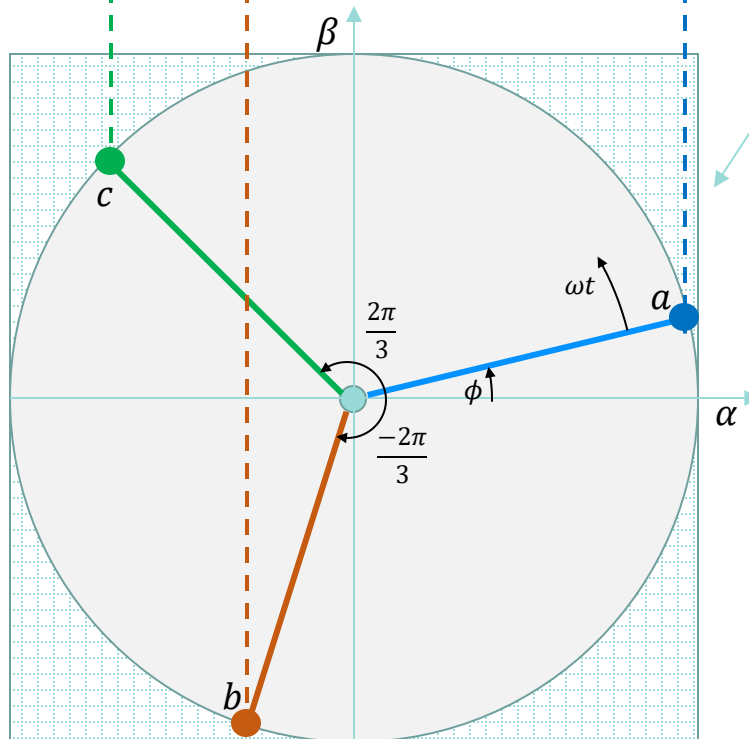


Digitized data – **millions** of recorded values

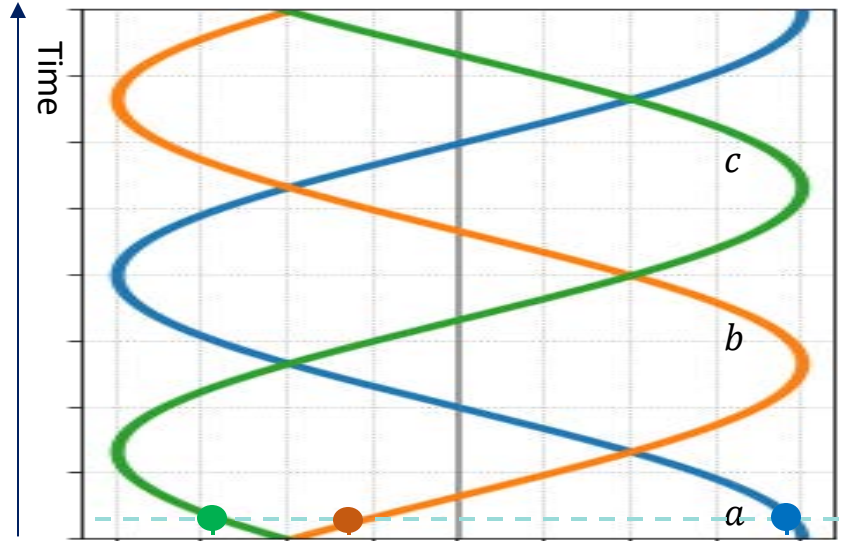
If all 'phases' are:

- sinusoidal
- equal & constant amplitude
- equal & constant angular spacing

then the locus of the phasor is circular



Direct Quadrature Transformation – α, β

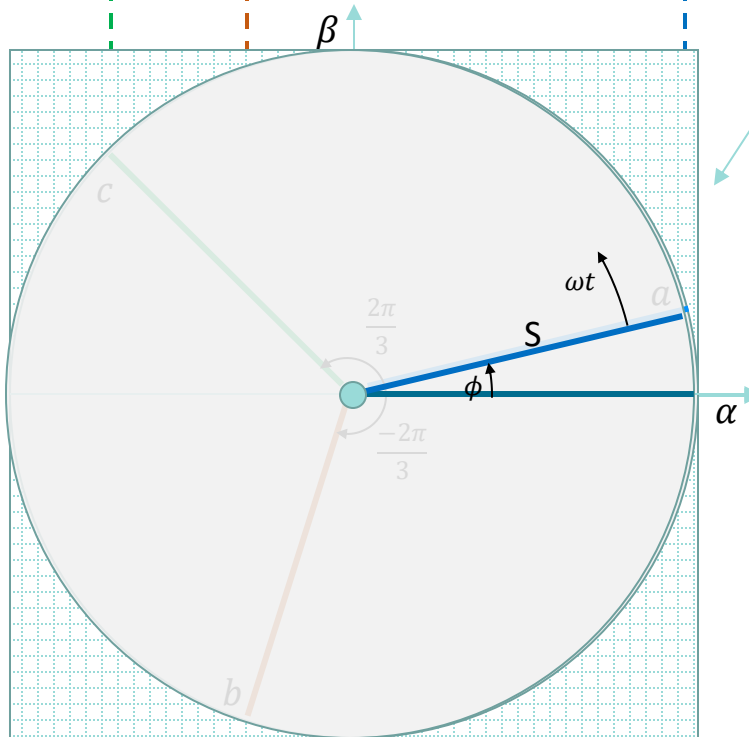


Digitized data – **millions** of recorded values

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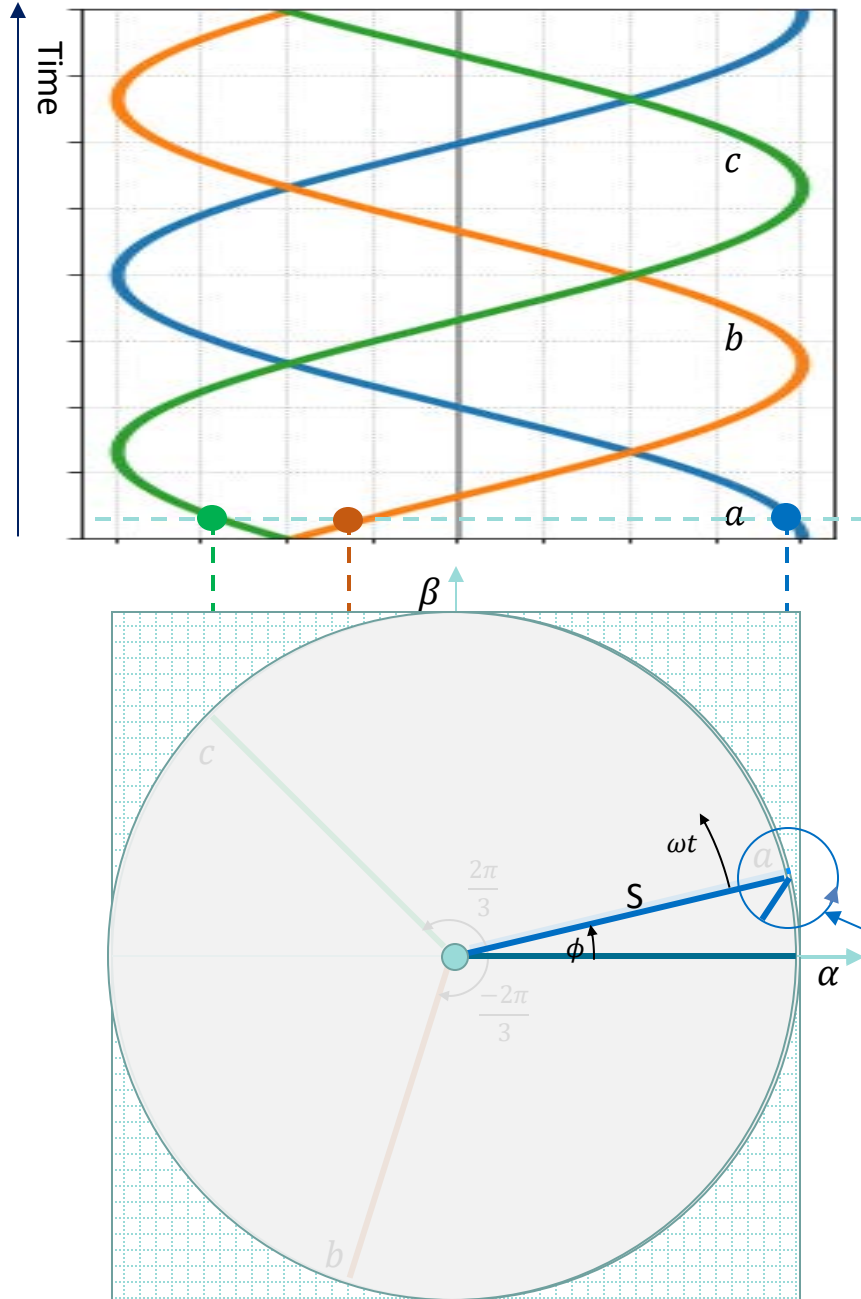
Polar coordinates

Digitized data completely described using just **3 values**:

- S – amplitude (radius of phasor)
- ϕ – initial phase angle (relative to some reference line α)
- ω – rotational frequency (or line frequency)



Direct Quadrature Transformation – α, β



Polar coordinates

E.g. Calculate power from voltage and current signals

$$p(t) = u(t) \times i(t)$$

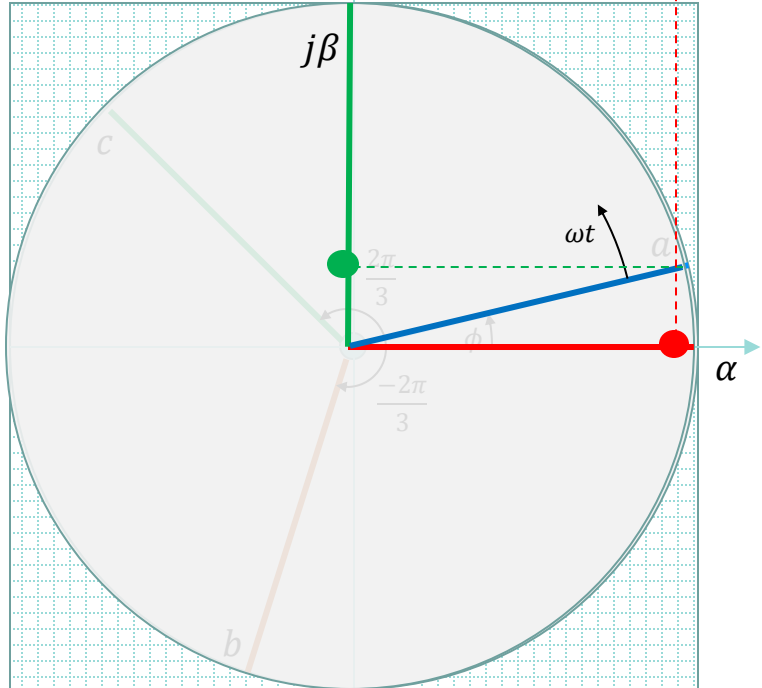
$$= S_u \cos(\omega t + \phi_u) \times S_i \cos(\omega t + \phi_i)$$

If $\phi_u = \phi_i$ then the power is wholly Active

If $\phi_i \neq \phi_i$ then the power will comprise a ratio of Active and Reactive components

Nice and easy
The basis for most hand calcs
No good for digitized data
Inflexible for changing waveforms
Doesn't easily support additional harmonics





Rectangular coordinates

Digitized data completely described using 2 values at each point

- $\alpha(t)$ – the x (or *Real* axis)
- $\beta(t)$ – the y (or *Imaginary* axis)

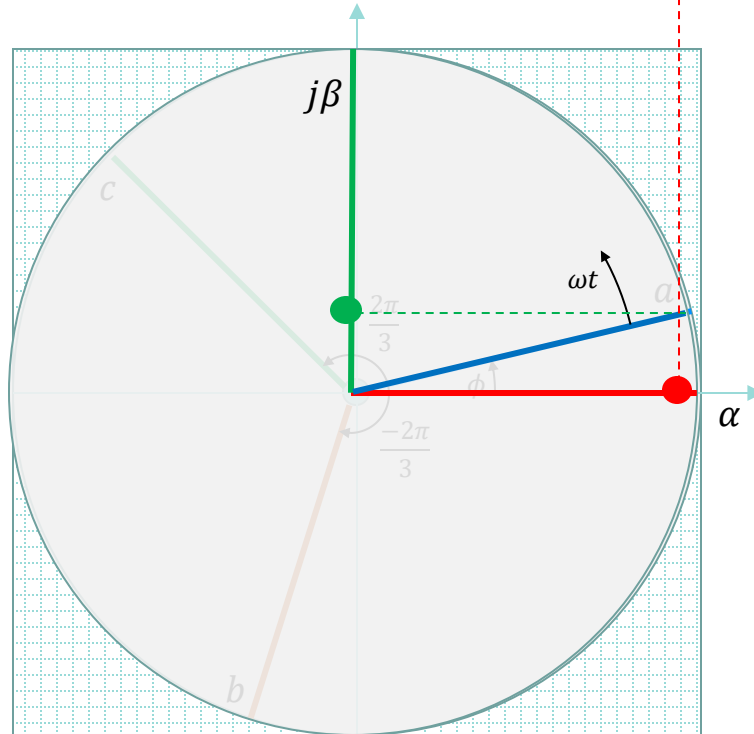
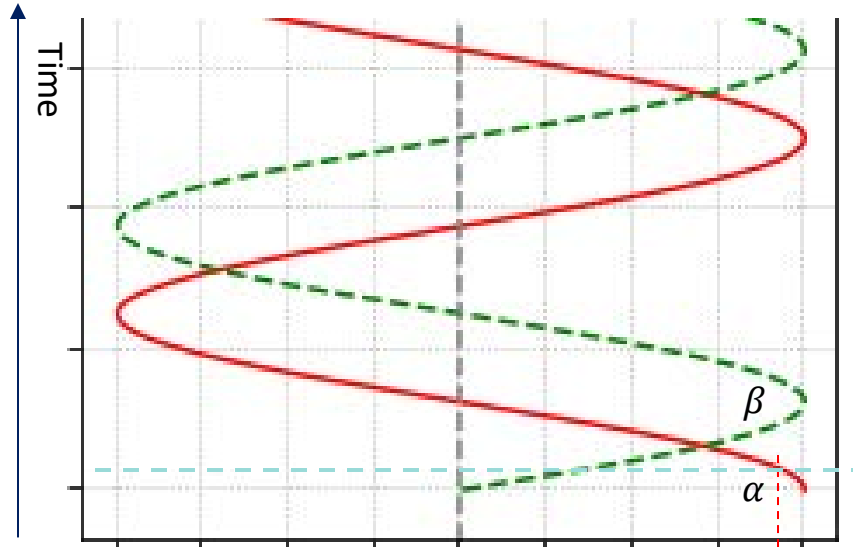
Pros and Cons

Cons: More values (α, β at each point)

Pros:

- Ideal for digitized data
- No need to assume
 - equal & constant amplitude S
 - equal & constant angular spacing
 - constant line frequency ω
- Phasor can change length with each point
- Phasor can move backward and forwards with changing ϕ
- Fast linear analysis using complex number theory

Direct Quadrature Transformation – α, β



E.g. Calculate power from voltage and current signals

$$\left[\textcolor{red}{P} + j \textcolor{green}{Q} \right] (t) = \underbrace{\left[\alpha_u + j \beta_u \right] (t)}_{\text{Complex voltage}} \times \underbrace{\left[\alpha_i - j \beta_i \right] (t)}_{\text{Complex current}}$$

Question:

How do we calculate α, β from the time signal of voltage and current?

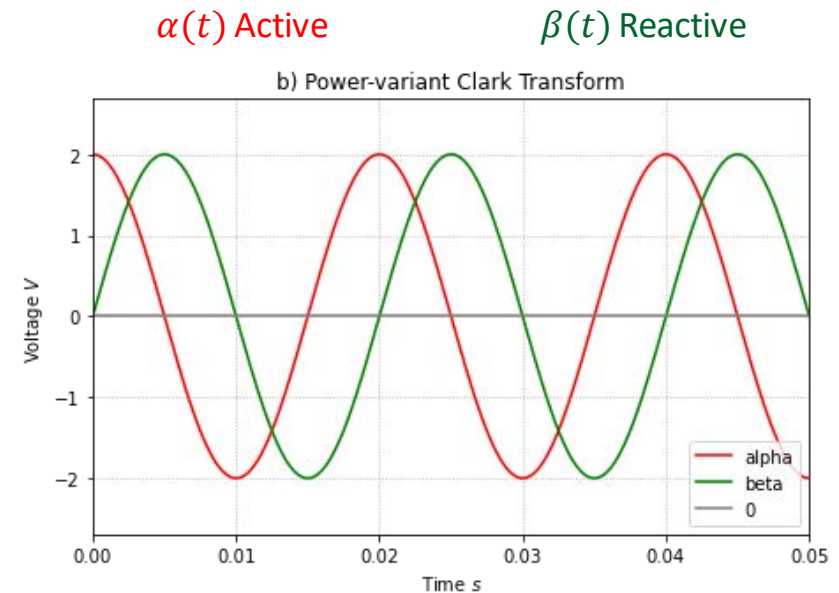
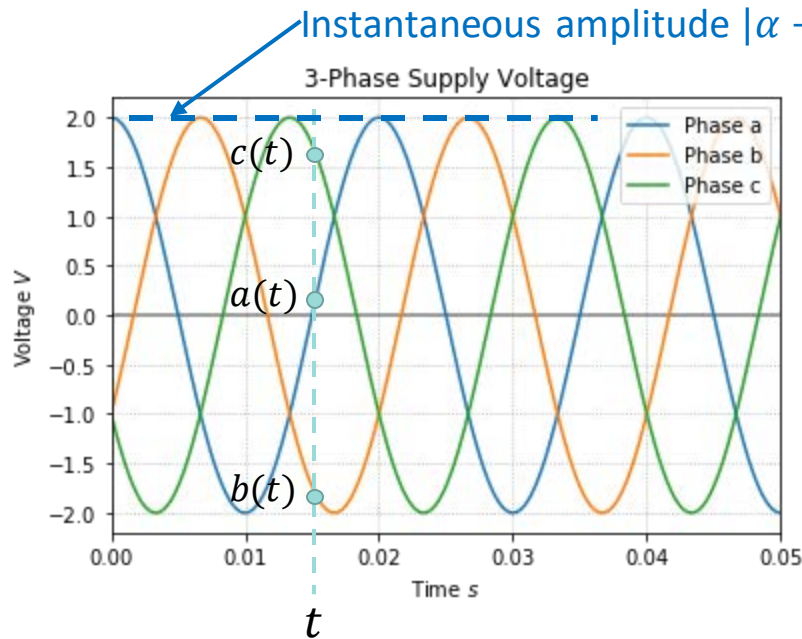
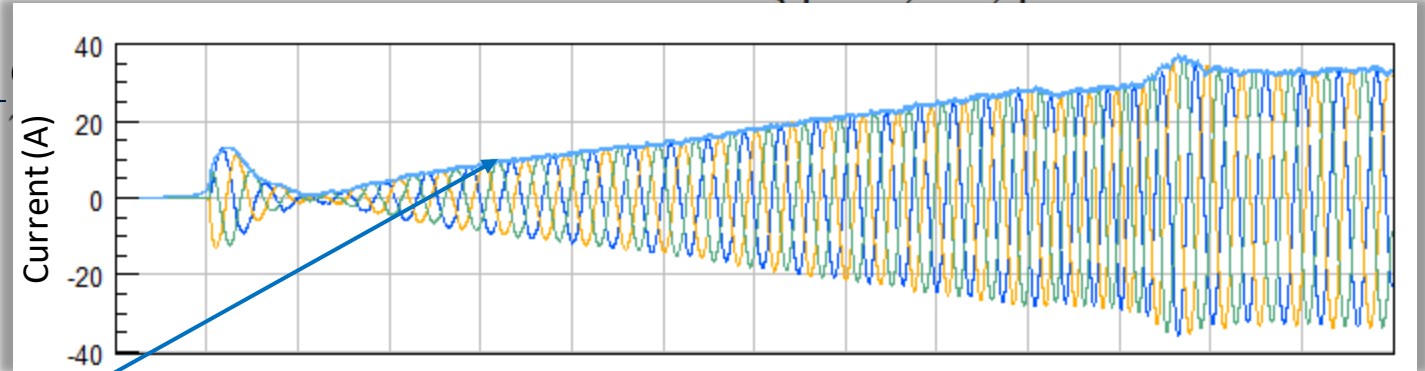
1. Clarke transform – *time domain*
2. Hilbert transform – *frequency domain*

Clarke transform – *time domain*

Uses all 3-phase values *simultaneously* to calculate α and β

- Assume all phases have same amplitude
- Assume phases are equally spaced (120°)
- Assume signals are sinusoidal
- Assume they do not change rapidly

$$\alpha = \frac{2}{3} \left[a - \frac{b}{2} - \frac{c}{2} \right]$$



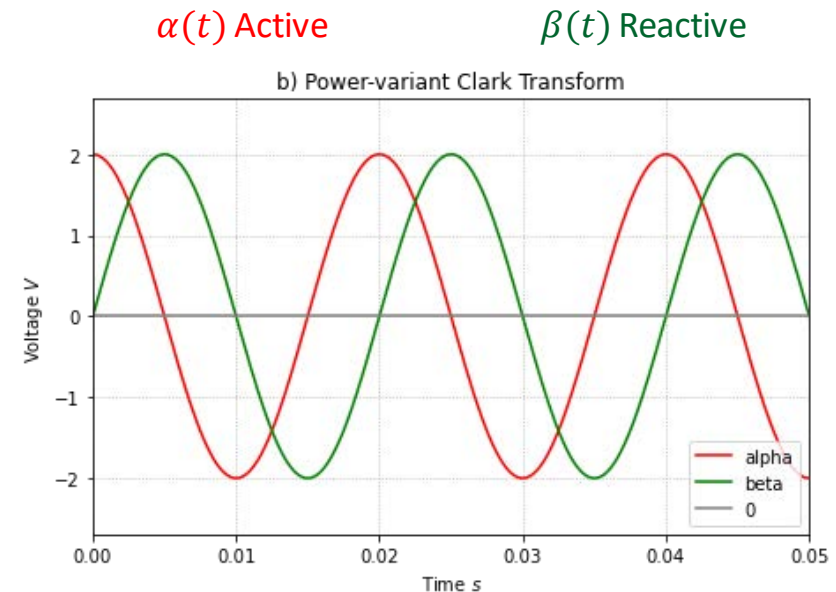
Hilbert transform – *frequency domain*

$$\left[\alpha_u + j \beta_u \right] (t) = \mathcal{F}^{-1} \left\{ \mathcal{H} \left[\mathcal{F} (u(t)) \right] \right\}$$

1. Fourier transform signal $\mathcal{F}[a(t)]$
2. Set all negative frequency components to zero $\mathcal{H}()$
3. Inverse Fourier transform $\mathcal{F}^{-1}()$
4. α is the real part and β is the imaginary

Hilbert Transform

- ▲ Uses Fourier to create α and β directly
 - Works on single phase at a time and combines them later
 - Suitable for single and multi-phase
 - Phases can be imbalanced
 - Waveforms can be non-sinusoidal
 - Waveforms can change rapidly



Comparing the Clarke and Hilbert Transforms

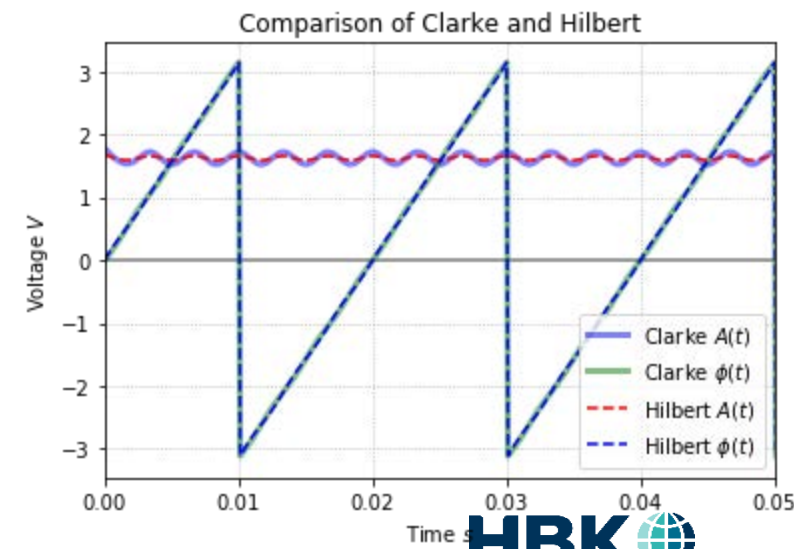
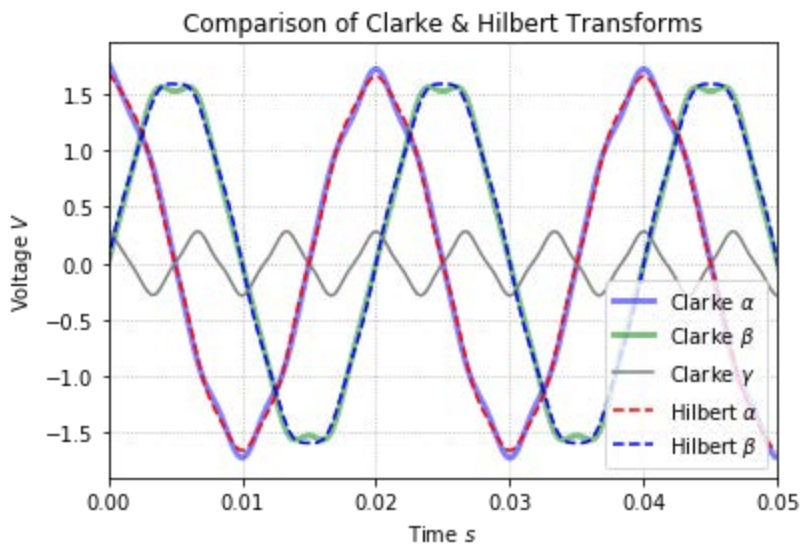
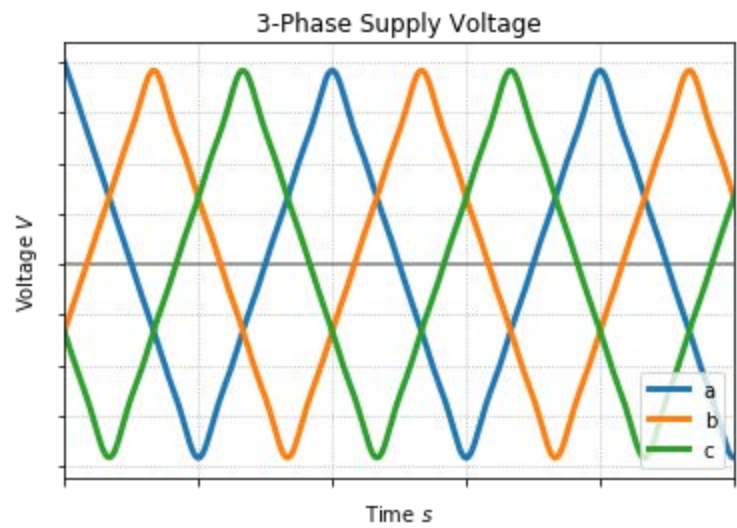
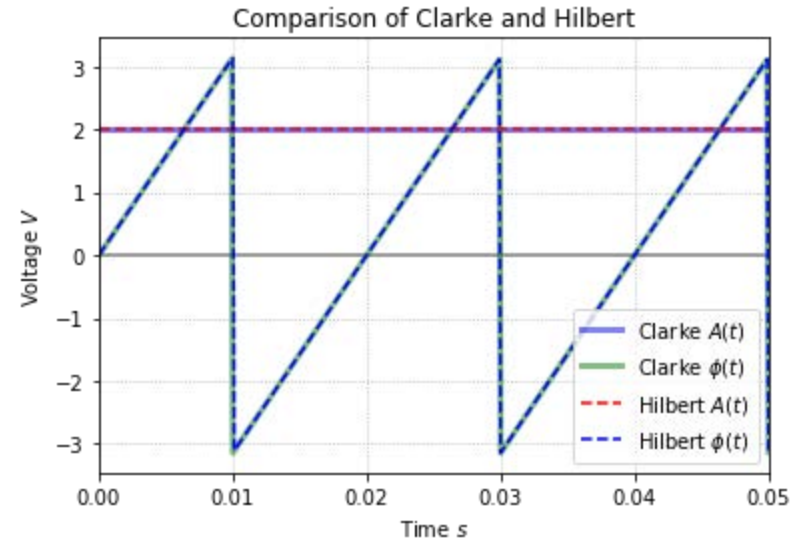
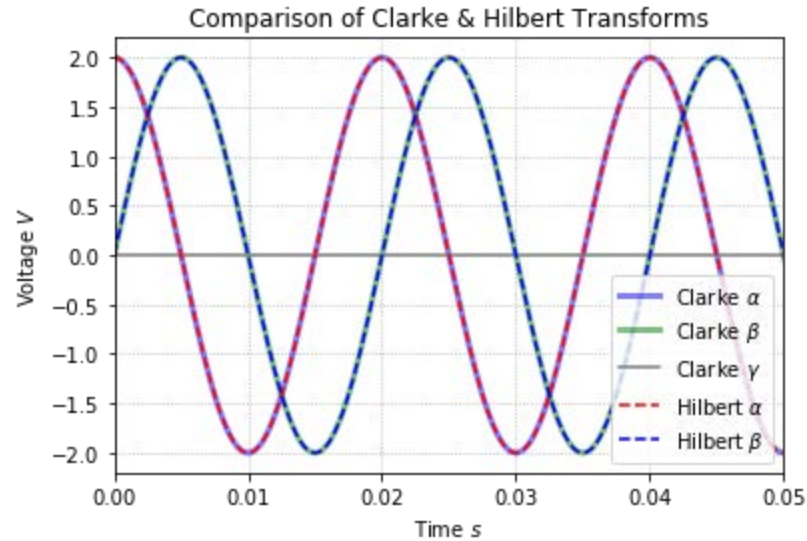
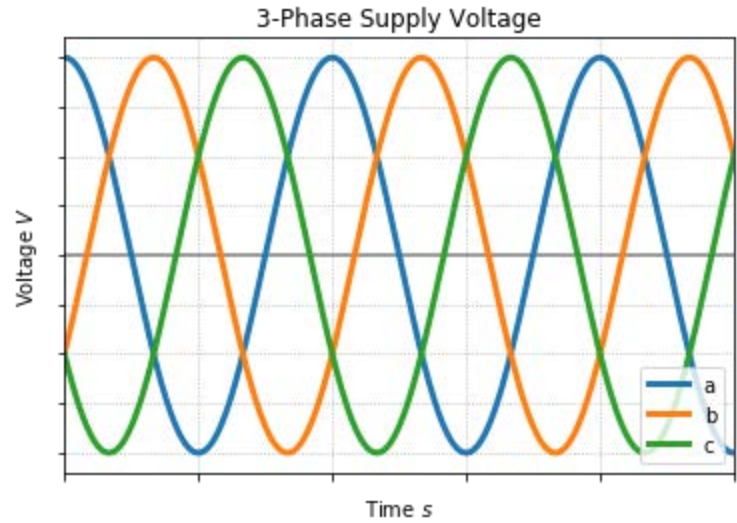
Clarke Transform – *time domain*

- ▲ Must be 3-phase
 - ▲ Must be sinusoidal
 - ▲ Must be balanced
 - equal & constant amplitude
 - equal & constant angular spacing
 - ▲ Must be stationary
-
- ▲ Suitable for real-time calculations
 - ▲ Often used for non-sinusoidal waves but suboptimal
 - ▲ Often used for non-stationary signals but suboptimal
 - ▲ There is a check for balance ($\gamma = 0$)

Hilbert Transform – *frequency domain*

- ▲ More complex computational analysis
 - Requires large FFT buffers
 - ▲ Unsuitable for real-time calculations must be off-line post-processed
-
- ▲ Fast
 - ▲ Suitable for single and multi-phase
 - ▲ Suitable for non-sinusoidal waves
 - ▲ Suitable for transient signals

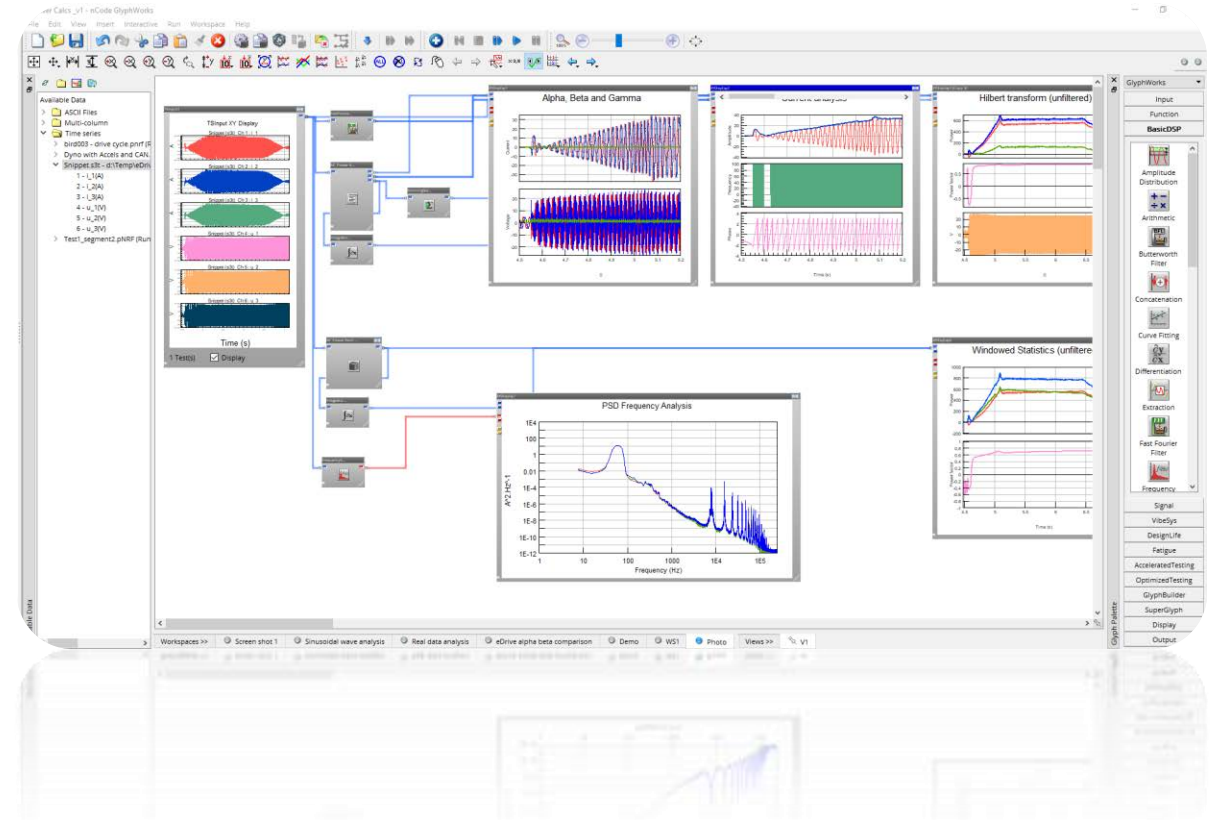
Comparing the Clarke and Hilbert Transforms



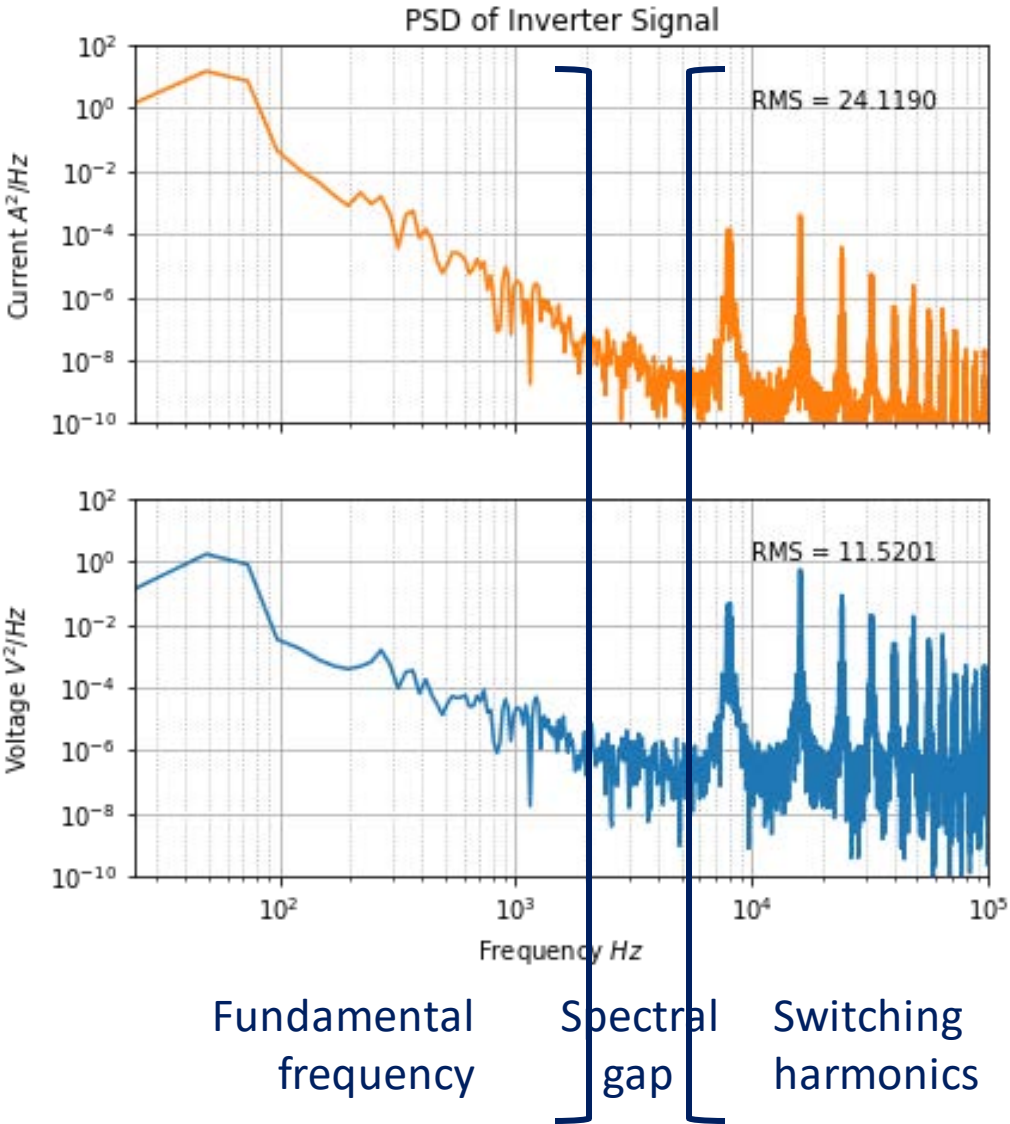
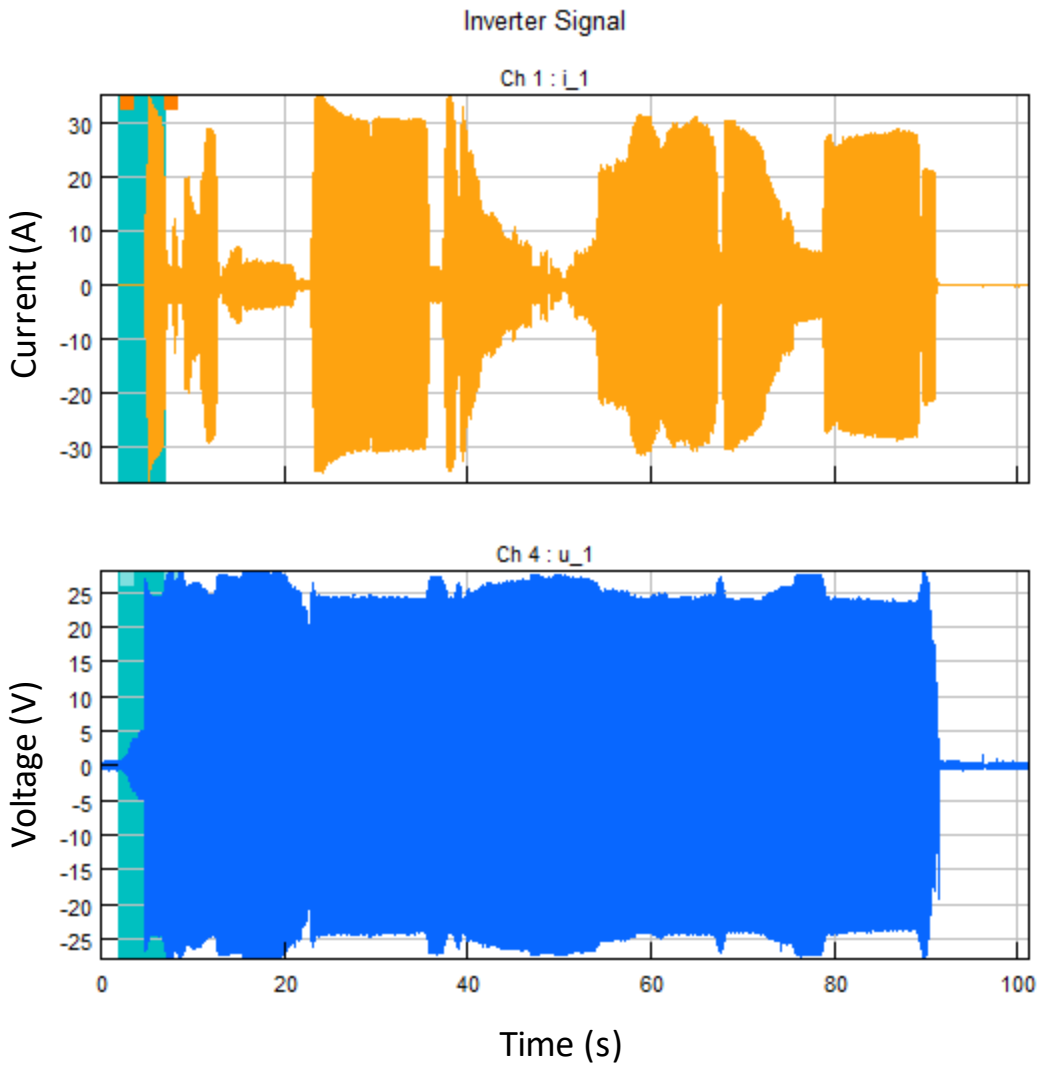
GlyphWorks Post-processing Case Studies

GlyphWorks EV Power Post Processing

1. An EV engineer wants to use the **Windowed Statistical Method** to calculate the power factors at the fundamental frequency
2. An EV engineer wants to compare the **Clarke** and **Hilbert** methods to calculate the power factors at the fundamental frequency
3. An EV engineer wants to use the **Hilbert** method to optimize the inverter switching profile



Measured Time Signal

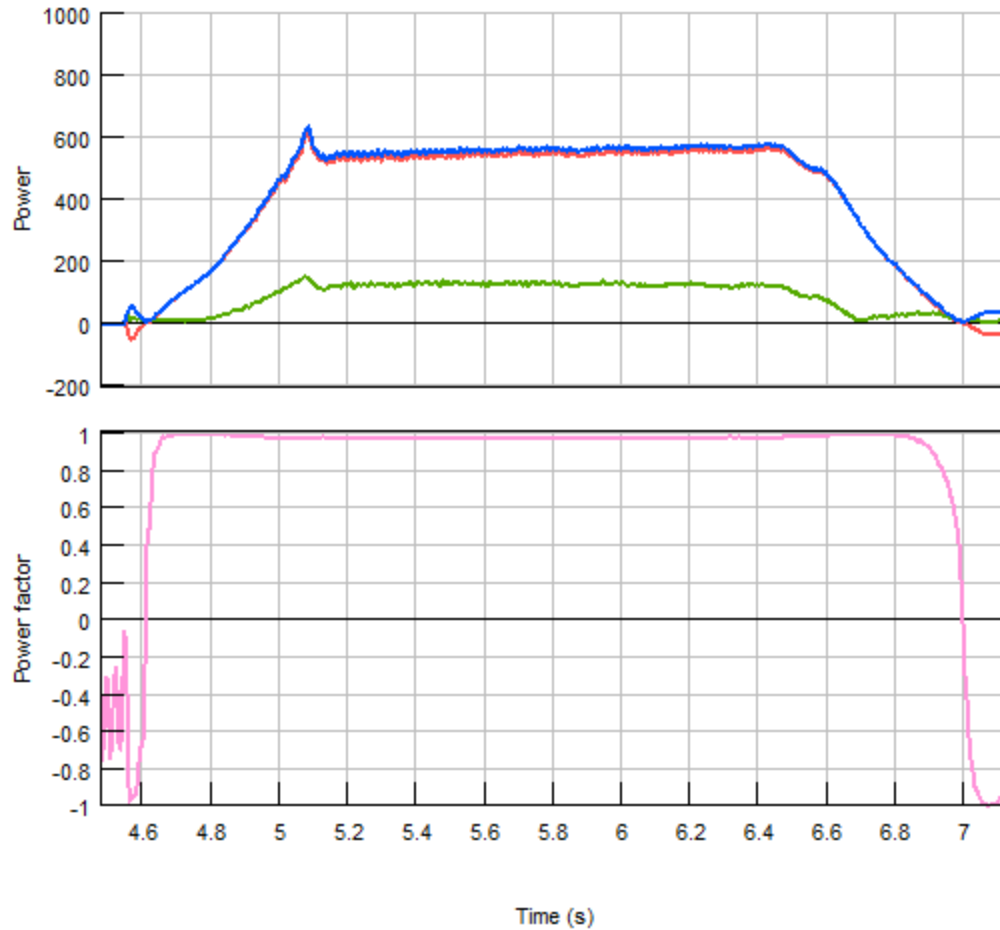


User Story 1

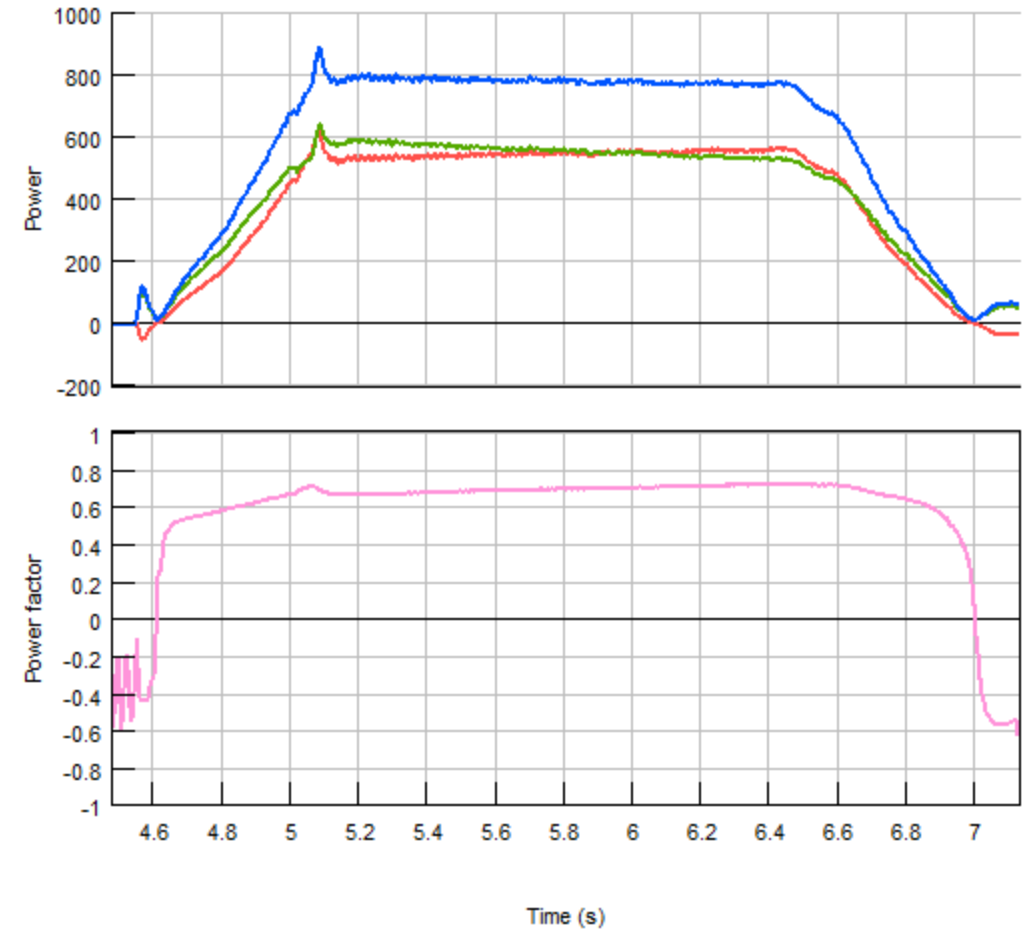
Active, Reactive, Apparent power

An EV engineer wants to use the **Windowed Statistical Method** to calculate the power factors at the fundamental frequency

Windowed Statistics (fundamental frequency)



Windowed Statistics (unfiltered)

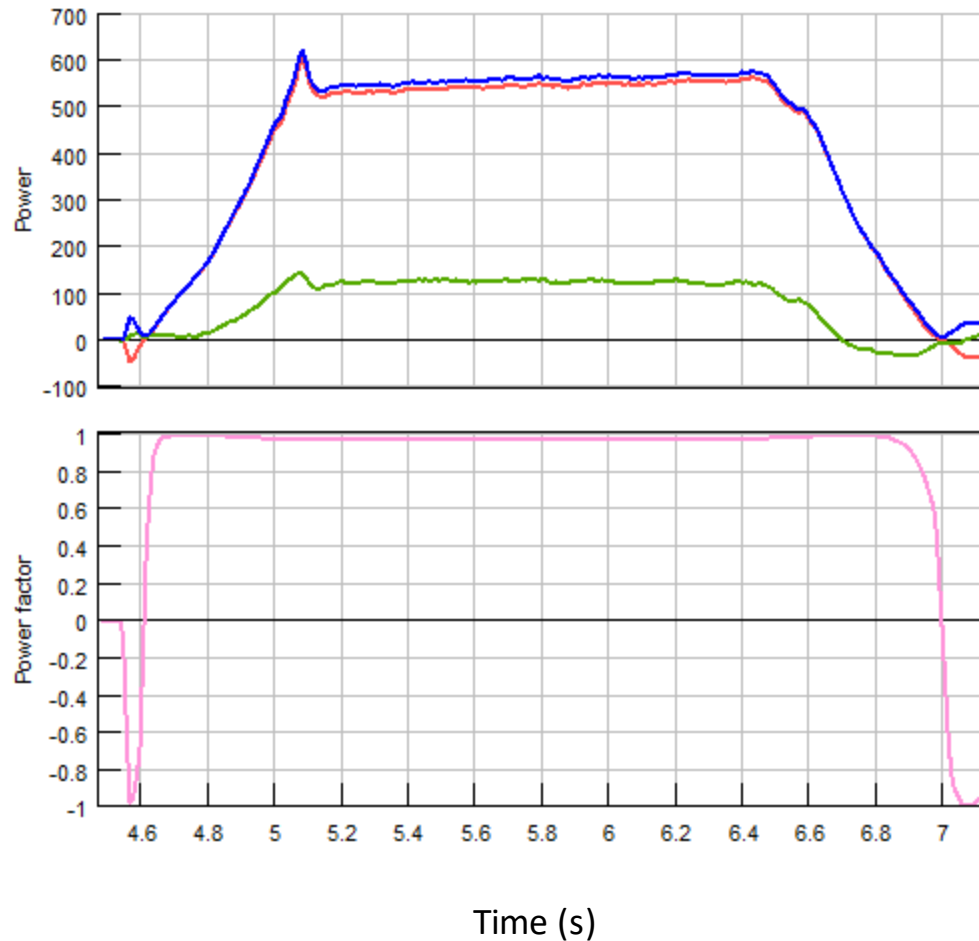


User Story 2

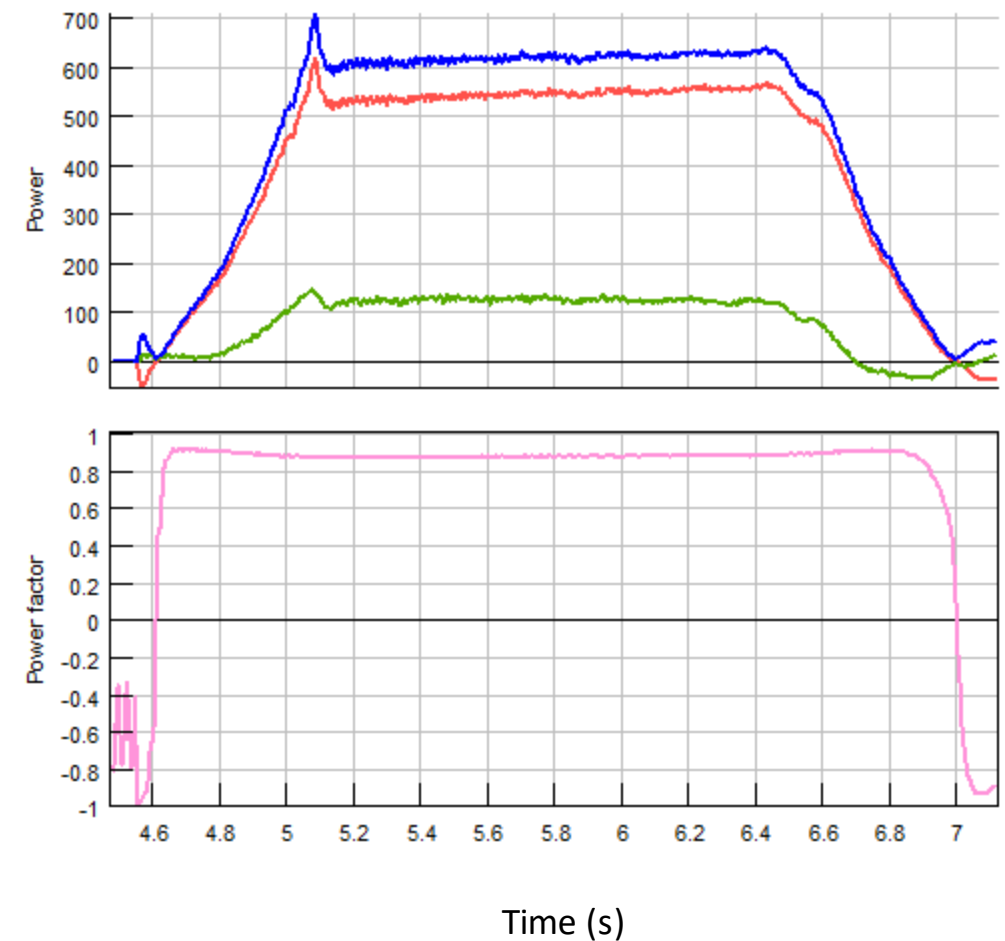
Active, Reactive, Apparent power

An EV engineer wants to compare the **Clarke** and **Hilbert** methods to calculate the power factors at the fundamental frequency

Clarke transform (fundamental frequency)



Clarke transform (unfiltered)

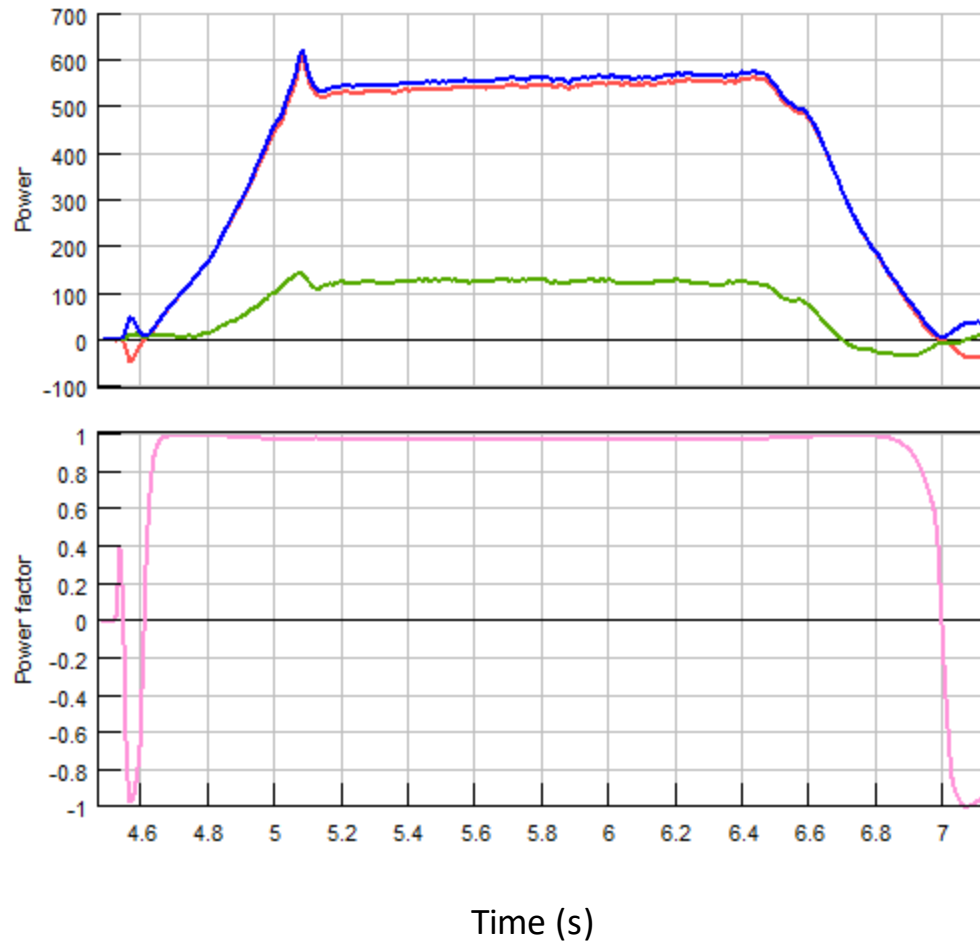


User Story 2

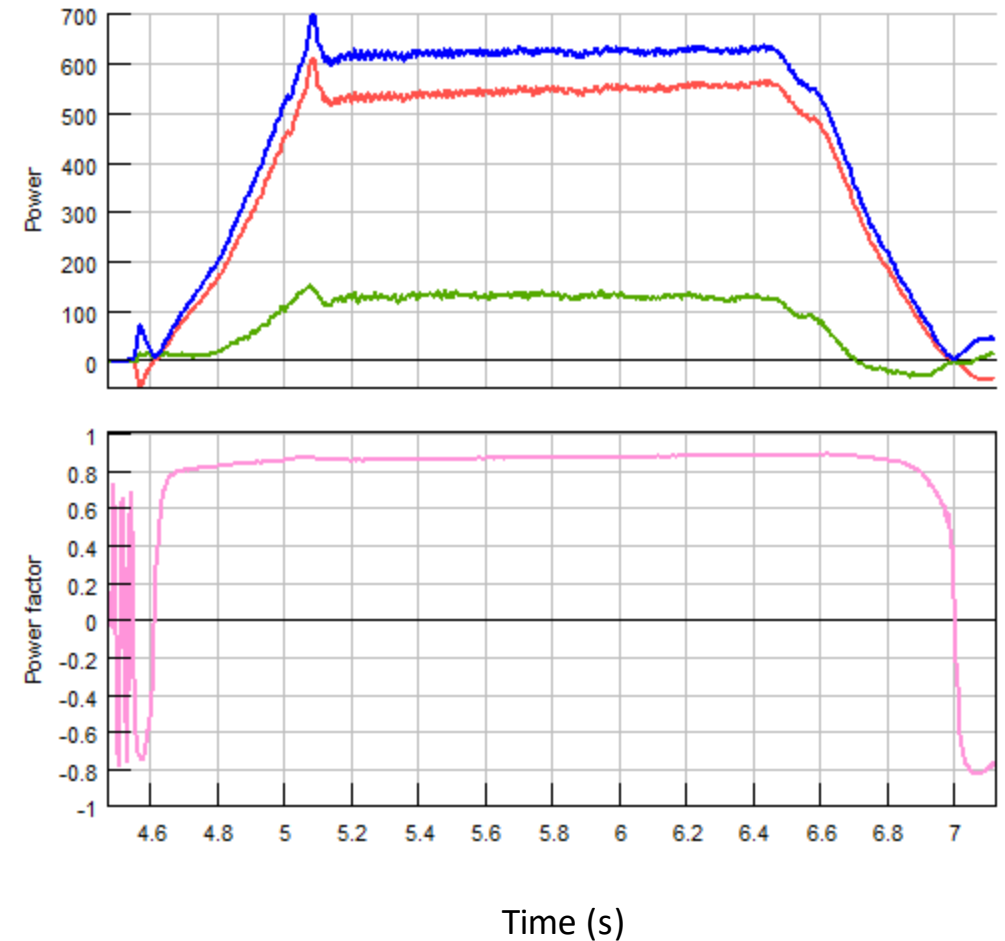
Active, Reactive, Apparent power

An EV engineer wants to compare the **Clarke** and **Hilbert** methods to calculate the power factors at the fundamental frequency

Hilbert transform (fundamental frequency)



Hilbert transform (unfiltered)

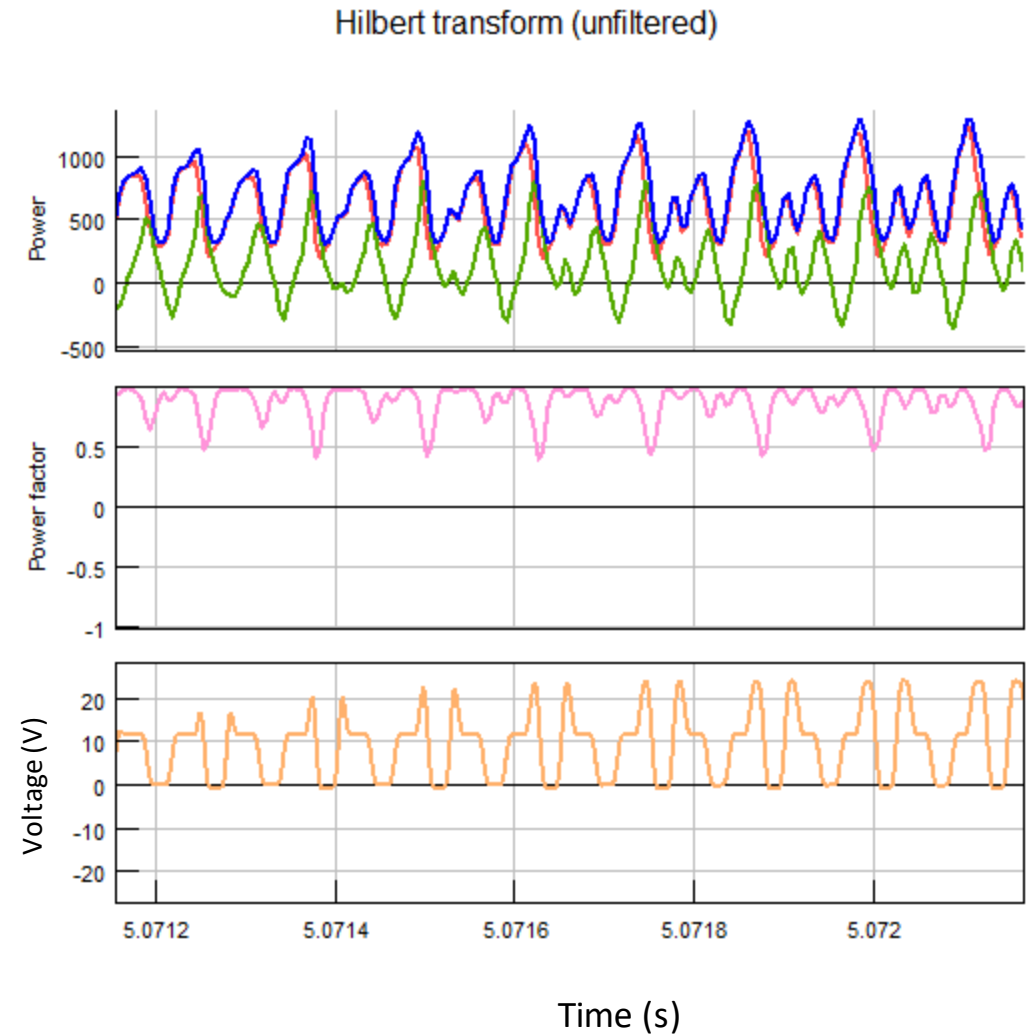
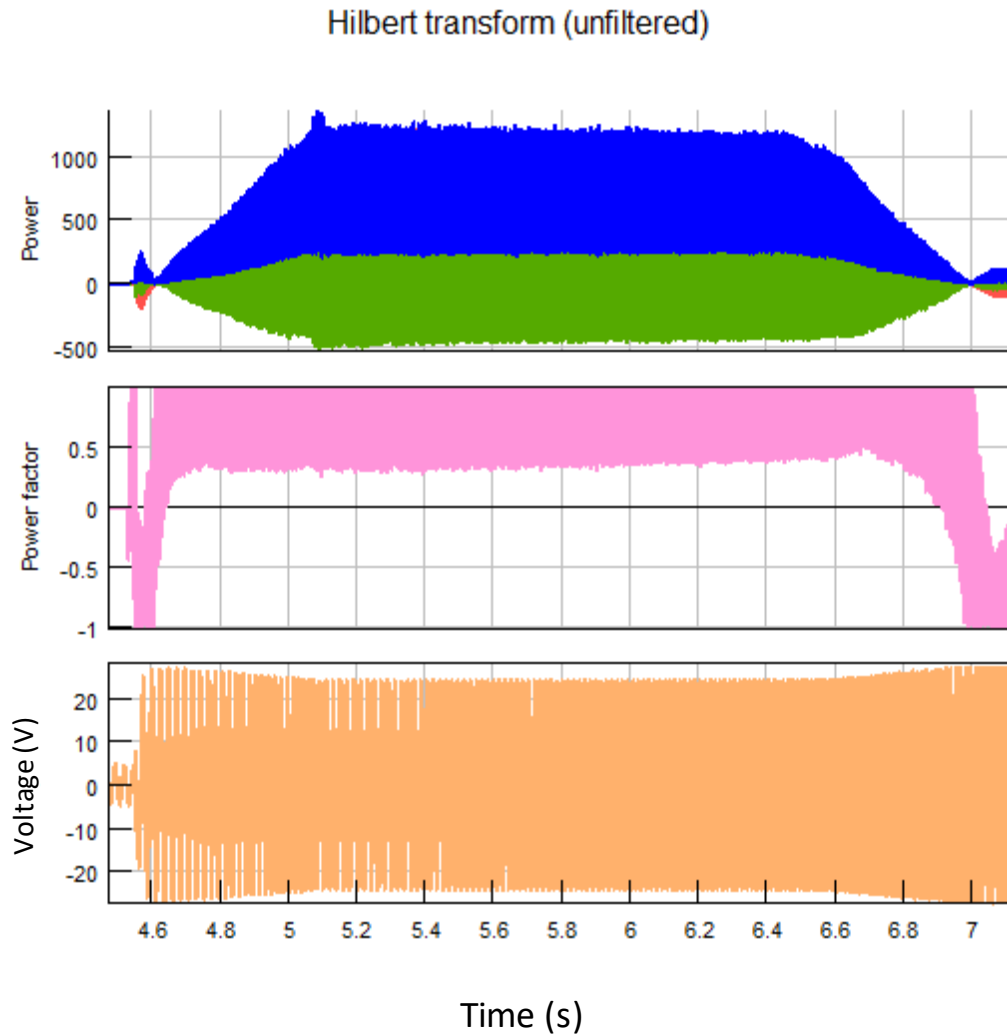


User Story 3

An EV engineer wants to use the **Hilbert** method to optimize the inverter switching profile

Active, Reactive, Apparent power

Progressively zoom-in to see switching effects



Conclusion

Conclusion

Definitions: Pure Sine AC

▲ Presentation Objective

- **Maximize EV efficiency** – AC Inverter/motor system

▲ Non-sinusoidal, dynamic AC power

- **Active** – consumed to drive the vehicle
- **Reactive** – not consumed but causes efficiency losses

▲ What we want

1. An **accurate** measurement of **Active** power to maximize
2. A **robust inference** of **Reactive** power to minimize

▲ Definitions - *Active, Reactive, Apparent & Power Factor*

- Analytical & Digital definitions
- Pure sine & broadband signals

Time-averaging methods

Fundamental frequency

▲ Windowed-statistical method – *time domain*

- Pure sine method
- **For preferred definition of Q, use low-pass filter to isolate the fundamental frequency**
- Excellent time resolution possible
(*down to half-cycle in the best systems*)
- Ideal for analysing dynamic EV systems & WLTC (*Worldwide Harmonised Light Vehicle Test Procedure*)



▲ PSD method – *frequency domain*

- Broadband method
- Large fft buffer gives poor time resolution
Not ideal for dynamic EV systems & WLTC



Conclusion

Instantaneous methods

Fundamental & inverter switching high-frequencies

Clarke transform method – *time domain*

- Suitable for **real-time** calculations
- Must be **3-phase**
- Ideally should be: sinusoidal, balanced & stationary

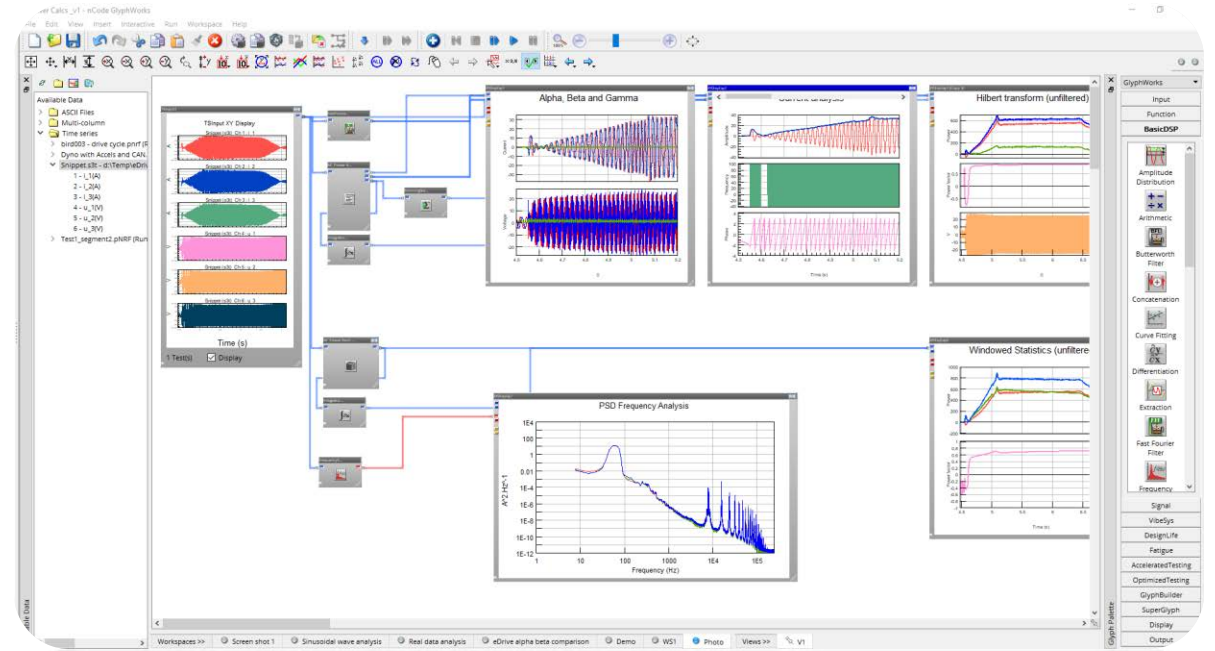


Hilbert transform method – *frequency domain*

- Unsuitable for real-time applications
- Suitable for single and **multi-phase**
- Suitable for **non-sinusoidal** waves
- Suitable for **dynamic** signals



GlyphWorks EV Power Post-processing



Thank You

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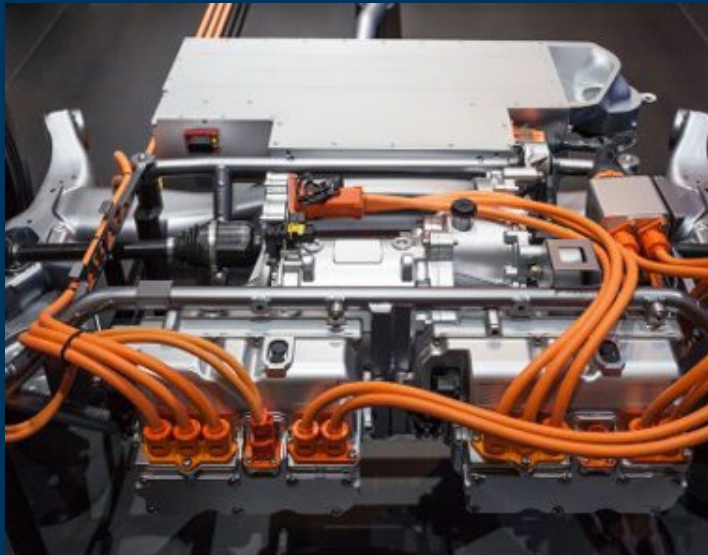
Q&A

▲ (no questions)



HBM Prenscia Technology Day

Virtual Seminar Series



Analysis of Electric Powertrain Measurements – Torque, Power, Efficiency, Vibration

Presented by Dr. Andrew Halfpenny
Chief Technologist, HBM Prenscia
HBK

Session #2: Electrical Power Testing & Analysis